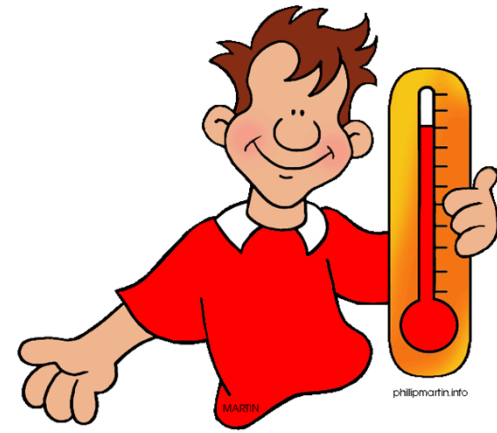
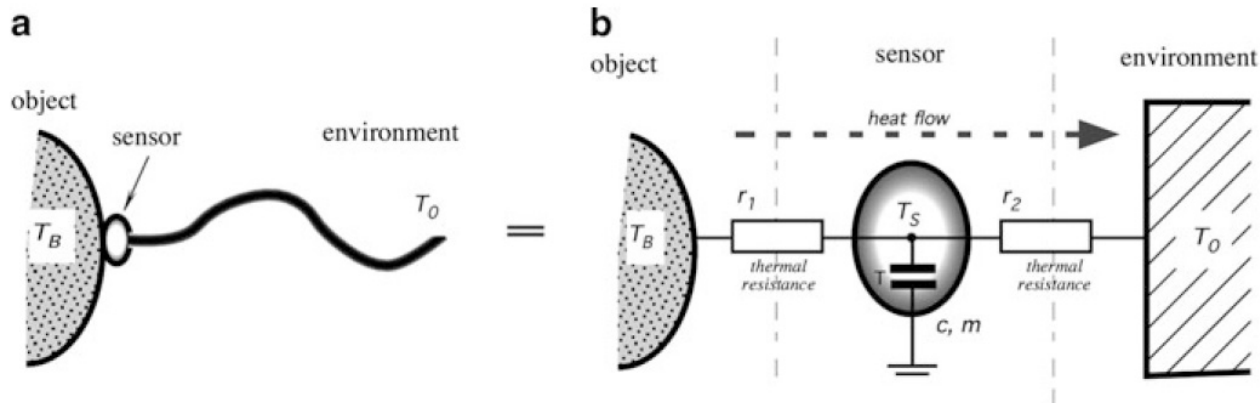


# Temperaturmåling

- Sensor-elementet mottar eller avgir varme i fht objektet
- Enten oppnås **likevekt**, dvs de får samme temperatur, eller så **predikeres** temperaturen ut fra endringsforløpet



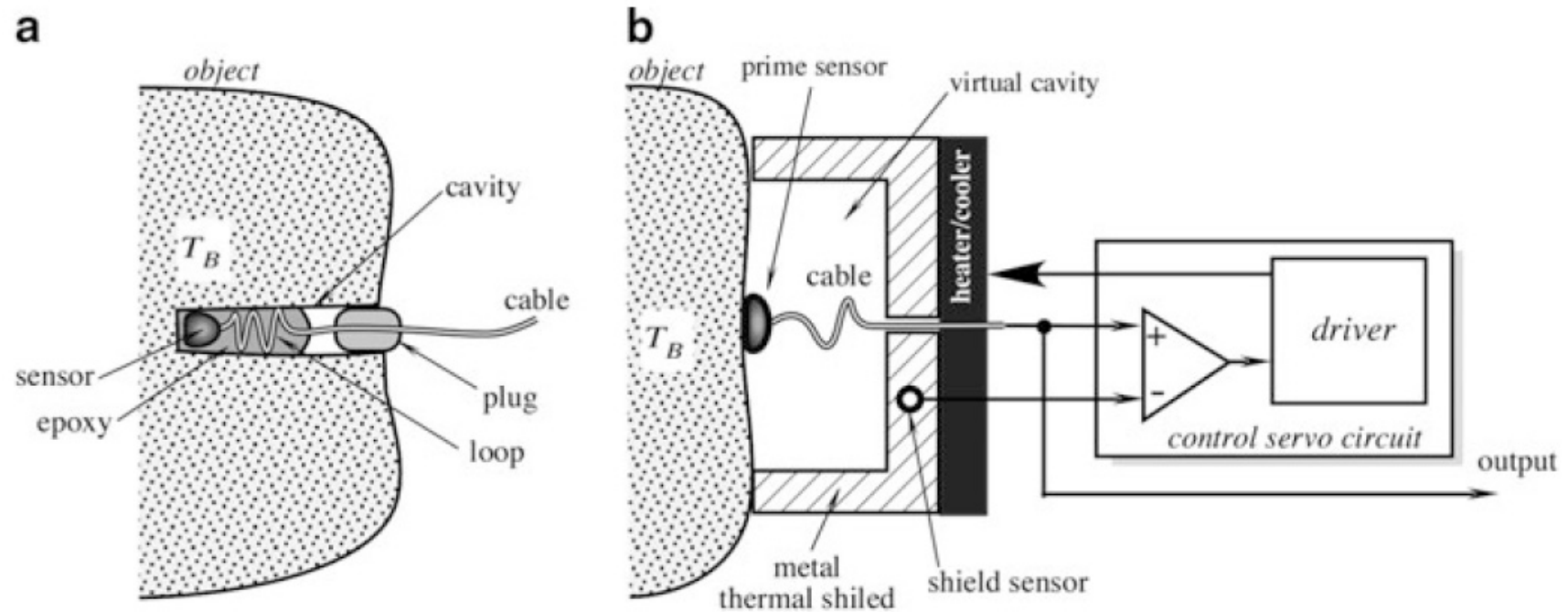
$$T_S = T_B - (T_B - T_0) \frac{r_1}{r_2} = T_B - \Delta T \frac{r_1}{r_2}$$



- $T_S \neq T_0$
- Poeng å redusere  $r_1$  og øke  $r_2$
- Kan redusere  $r_1$  (og øke  $r_2$ ) ved å bygge sensoren inn i objektet

**Fig. 16.1** Temperature sensor has thermal contacts with both the object and the connecting cable (a); equivalent thermal circuit (b)

# Innebygget sensor



**Fig. 16.2** Imbedded temperature sensor (a) and surface temperature sensor with an active driven thermal shield (b)

$$dQ = \alpha_1(T_B - T_S)dt, \quad (16.3)$$

where  $\alpha_1 = 1/r_1$  is the thermal conductivity of the sensor–object boundary. Note that  $T_s$  is changing. If the sensor has an average specific heat  $c$  and mass  $m$ , the heat absorbed by the sensor is

$$dQ = mcdT. \quad (16.4)$$

Equations (16.3) and (16.4) are equal and yield the first-order differential equation

$$\alpha_1(T_B - T_s)dt = mcdT. \quad (16.5)$$

We denote thermal time constant  $\tau_T$  as

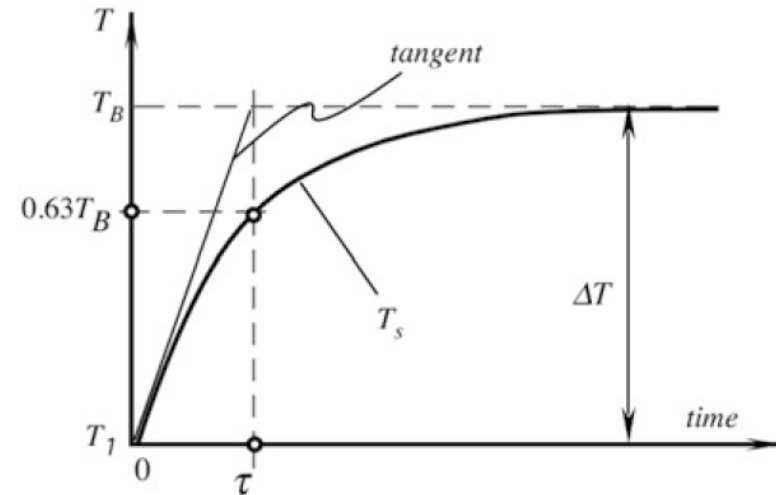
$$\tau_T = \frac{mc}{\alpha_1} = mcr_1,$$

then the differential equation takes form

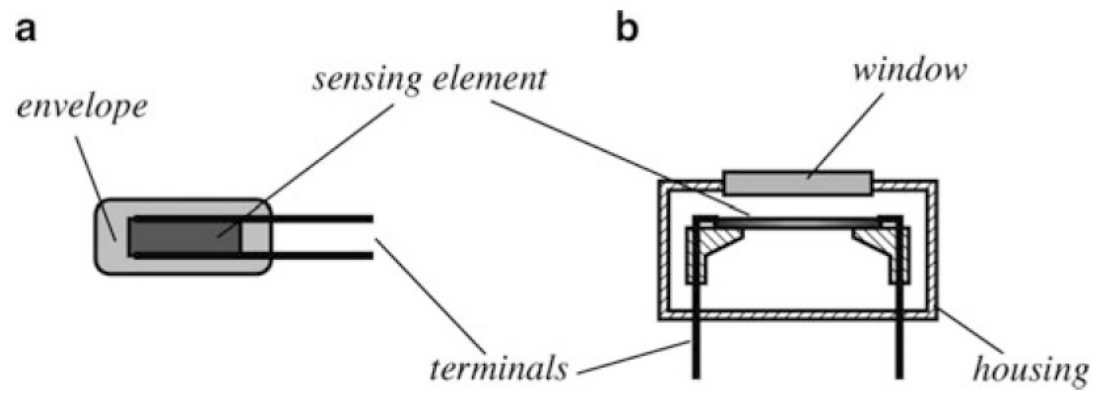
$$\frac{dT}{T_B - T_s} = \frac{dt}{\tau_T}.$$

This equation has a solution

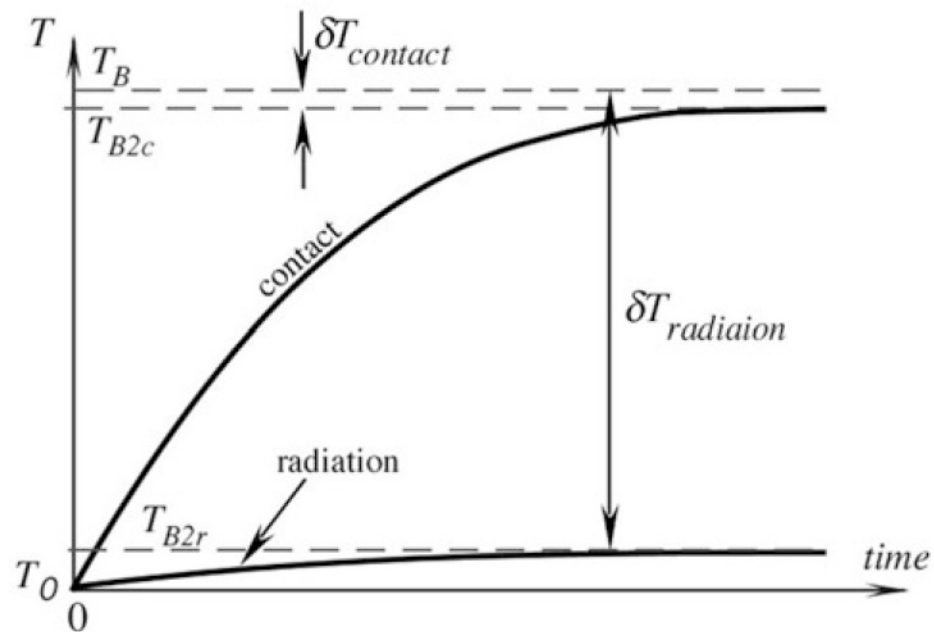
$$T_s = T_B - \Delta T e^{-\frac{t}{\tau_T}}. \quad (16.8)$$



**Fig. 16.3** Temperature changes of a sensor (the sensor is ideally coupled to an ideal object)



**Fig. 16.6** General structures of temperature sensors: Contact sensor (a) and noncontact thermal IR radiation sensor (b)



**Fig. 16.5** Difference in thermal responses between contact and noncontact (IR radiation) temperature sensors

# Temperatur -referanser



Point description	°C
Triple point <sup>a</sup> of hydrogen	-259.34
Boiling point of normal hydrogen	-252.753
Triple point of oxygen	-218.789
Boiling point of nitrogen	-195.806
Triple point of argon	-189.352
Boiling point of oxygen	-182.962
Sublimation point of carbon dioxide	-78.476
Freezing point of mercury	-38.836
Triple point of water	0.01
Freezing point of water (water-ice mixture)	0.00
Boiling point of water	100.00
Triple point of benzoic acid	122.37
Freezing point of indium	156.634
Freezing point of tin	231.968
Freezing point of bismuth	271.442
Freezing point of cadmium	321.108
Freezing point of lead	327.502
Freezing point of zinc	419.58
Freezing point of antimony	630.755
Freezing point of aluminum	660.46
Freezing point of silver	961.93
Freezing point of gold	1,064.43
Freezing point of copper	1,084.88
Freezing point of nickel	1,455
Freezing point of palladium	1,554
Freezing point of platinum	1,769

<sup>a</sup>Triple point is equilibrium between the solid, liquid, and vapor phases.

# Termoresistive sensorer

- Tre typer

- Resistance Temperature Detectors (RTD)

- Metaller. Alltid PTC. Pt mye brukt. Wolfram brukes over 600 °C

- Semiconductor (PN-junction) Detectors

- Si er egentlig NTC, men hvis dopet har det PTC ved lavere temperaturer. Typisk 0.7 % pr. °C

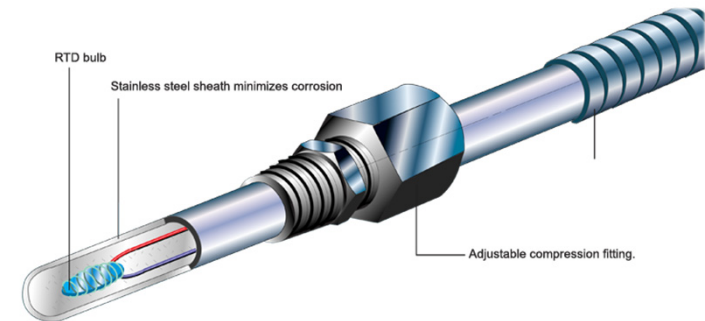
- Thermistors (keramer eller polymer)

- Både NTC (best) og PTC
- Resistans S:

$$\ln S = A_0 + \frac{A_1}{T} + \frac{A_2}{T^2} + \frac{A_3}{T^3}$$

- Tre metoder:

- **Simple method.** De to siste leddene fjernes. Enkel og god.
- **Fraden model.** To siste ledd fjernes og andre ledd modifiseres. Mer nøyaktig men fortsatt rimelig.
- **Steinhart-Hart model.** Nest siste ledd fjernes. Mest nøyaktig og dyrere (mer kalibrering er påkrevd).



RTD (Resistance Temperature Detector)

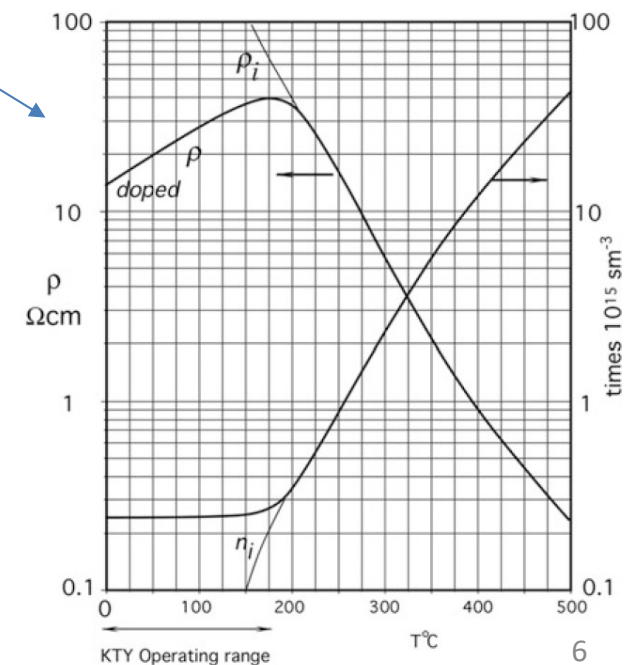
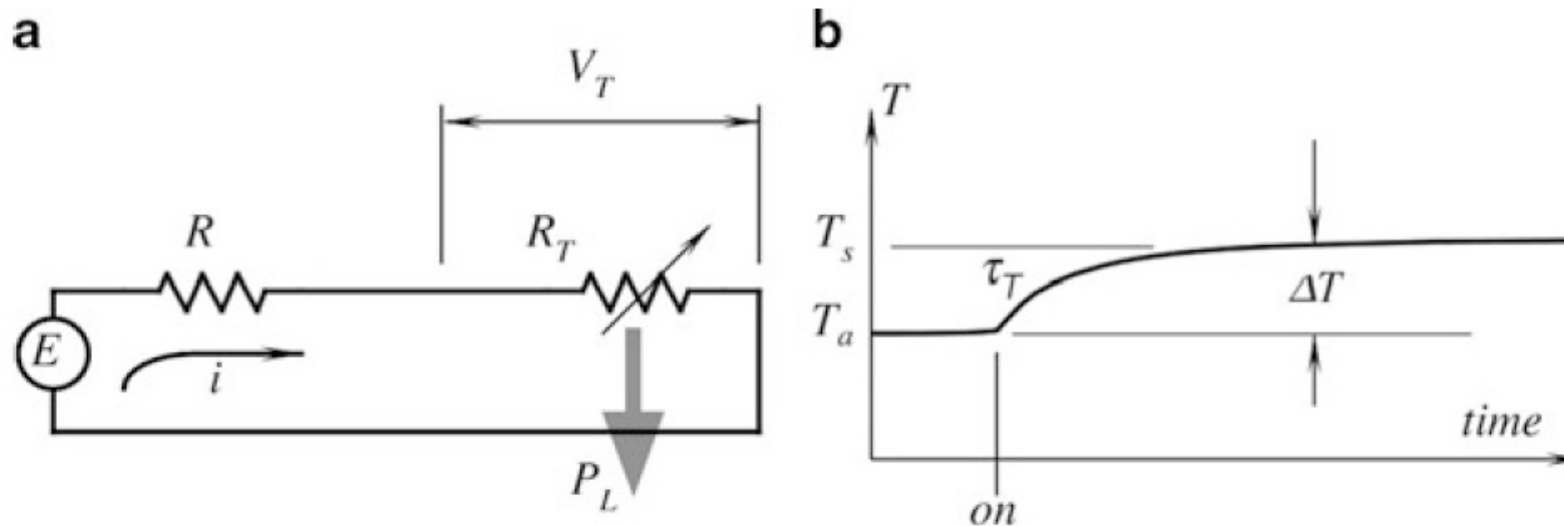


Fig. 16.7 Resistivity and number of free charge carriers for *n*-doped silicon



# Selvoppvarming av NTC termistorer

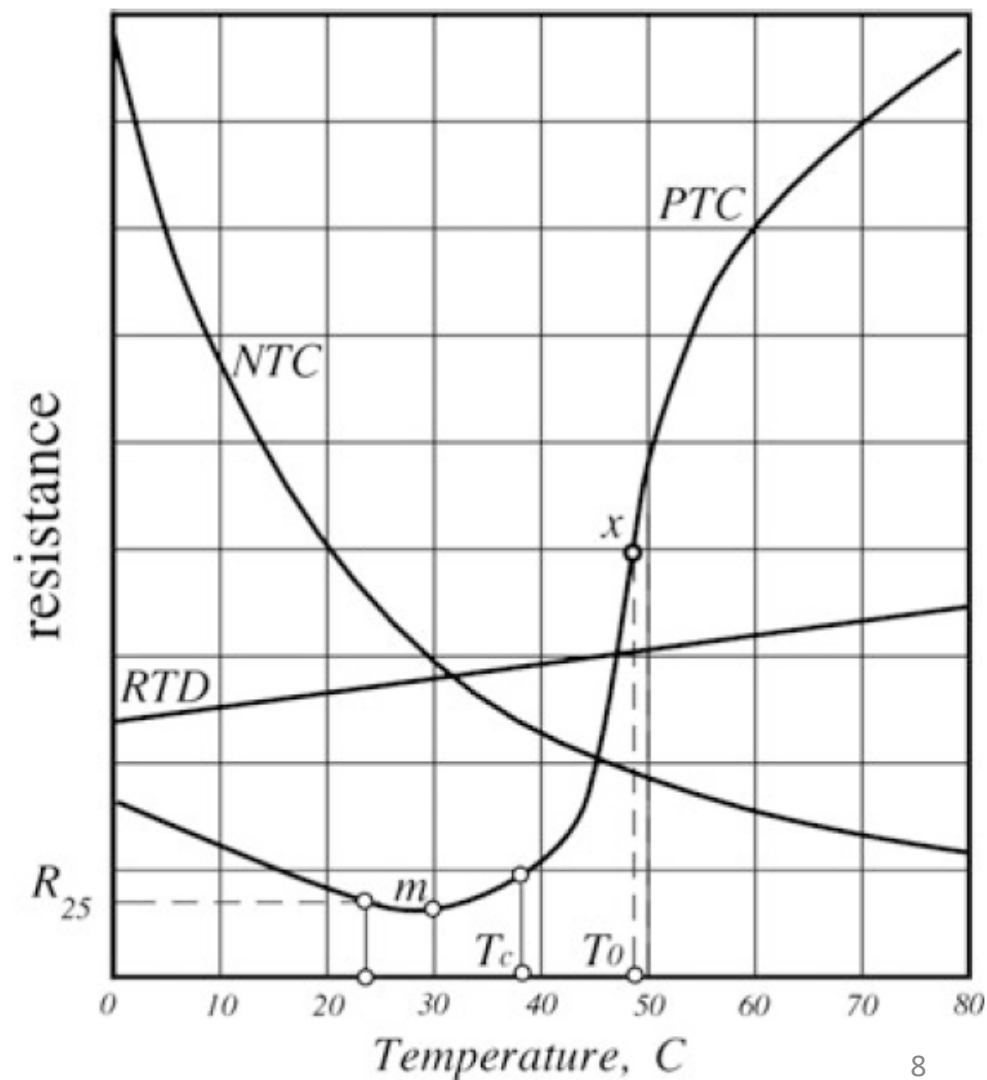
- Brukes aktivt i noen sensorer (strømning, termisk stråling, osv)
- Får en positiv-feedback-effekt hvis ikke effekten holdes under en viss grense.



**Fig. 16.13** Current passing through thermistor causes self-heating (a) and temperature of thermistor rises with thermal time constant  $\tau_T$ .  $P_L$  is thermal power lost to surroundings (b)

# PTC-termistorer

- Alle metaller har PTC (men er lite sensitive)
- Noen keramer har PTC og er veldig sensitive





# Thermocouples / thermopiles

## Termoelektriske lover:

1. Homogen krets + varme  $\neq$  strøm  
uansett kombinasjon av materialer
2. Alle junctions på samme temperatur  $\rightarrow$  ingen strøm
3.  $V_{13} = V_{12} + V_{23}$

Thermocouple-spenninger er små  $\rightarrow$  thermopile

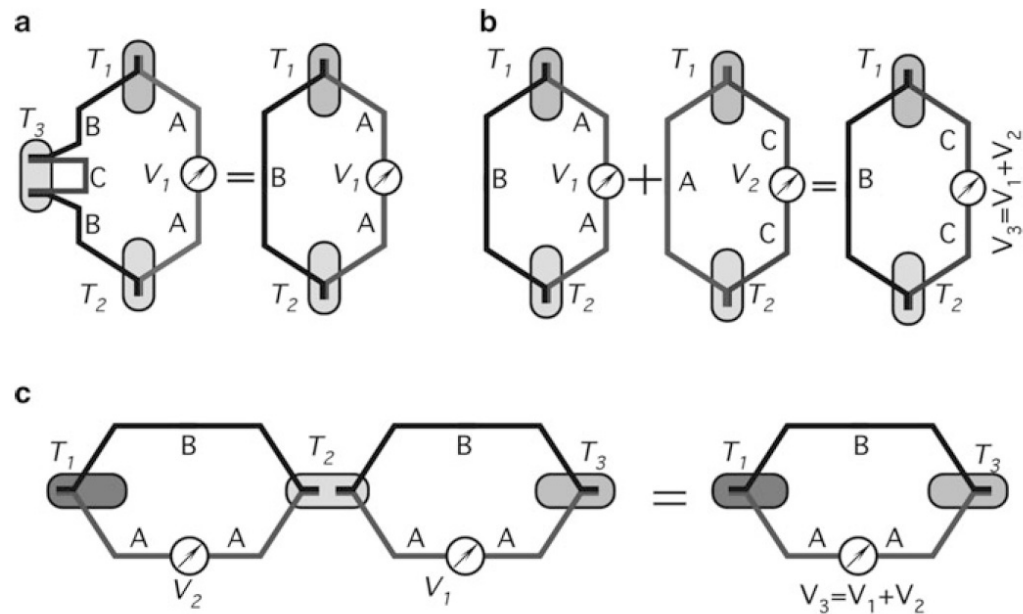


Fig. 16.18 Illustrations for the laws of thermocouples

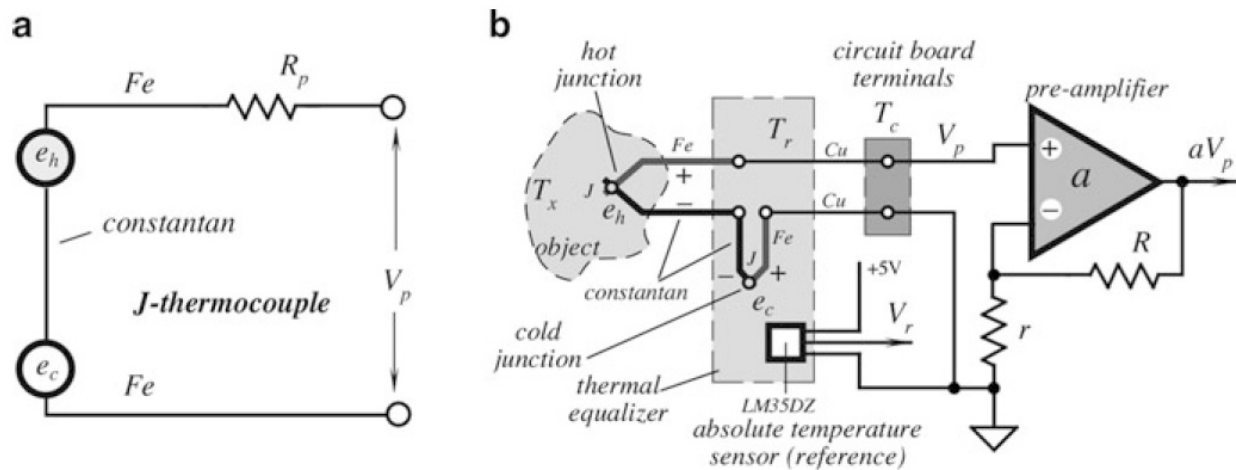
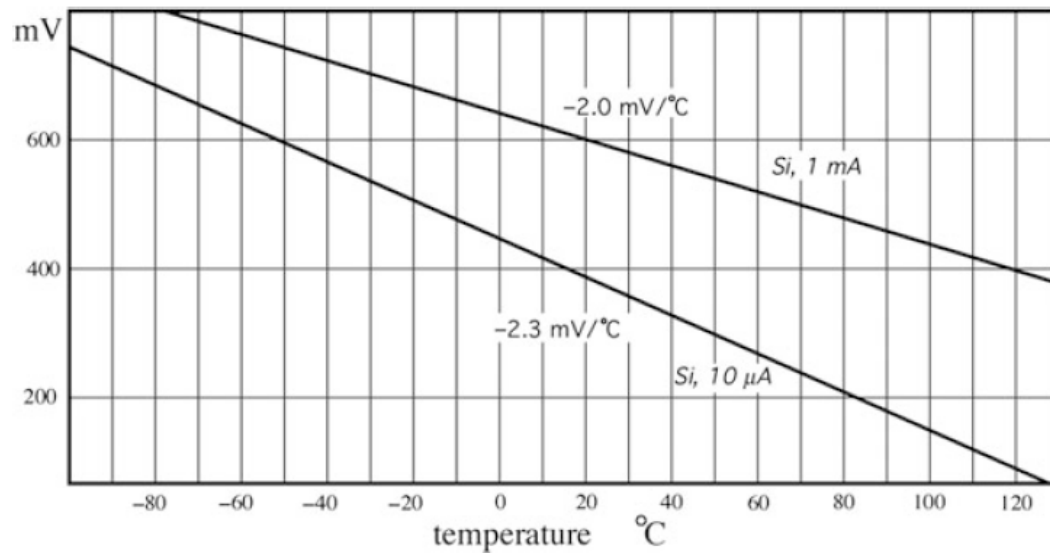


Fig. 16.19 Use of a thermocouple equivalent circuit of a thermocouple (a) and front end of a thermometer with a semiconductor reference sensor (b)

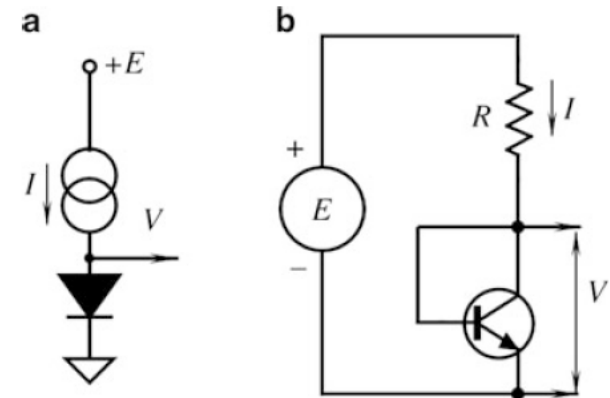
# Halvleder-overgang-sensor

- Veldig lineær sammenheng



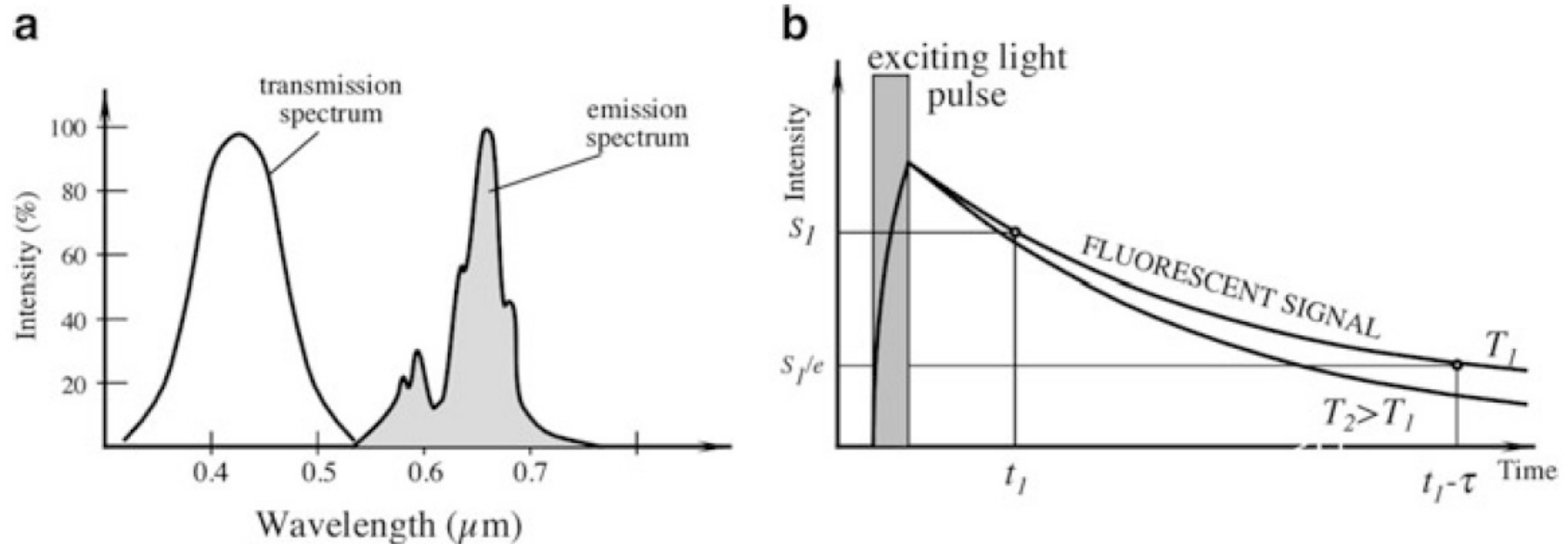
**Fig. 16.22** Voltage-to-temperature dependence of a forward biased semiconductor junction under constant current conditions

**Fig. 16.23** Forward biased  $pn$ -junction temperature sensors Diode (a) and diode-connected transistor (b)



# Optiske sensorer: Fluoro-optisk

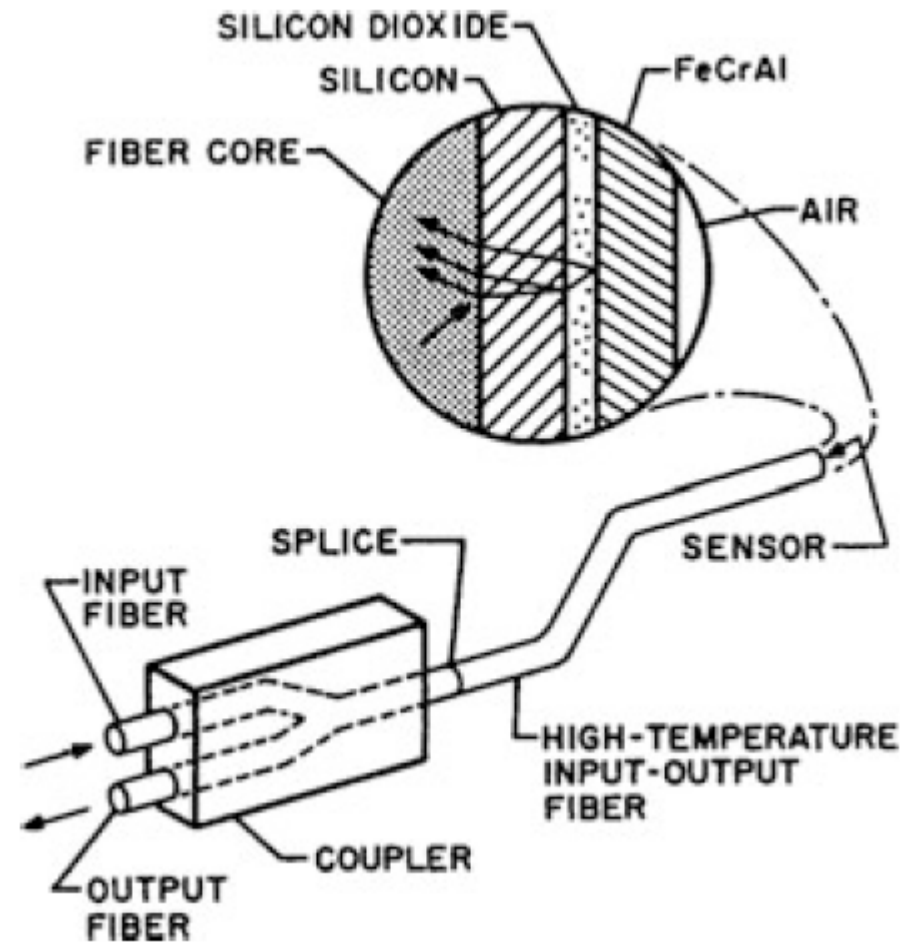
- Etterglødingen er avhengig av temperaturen
- Bruker ofte fosfor
- Belyses med UV eller blått lys

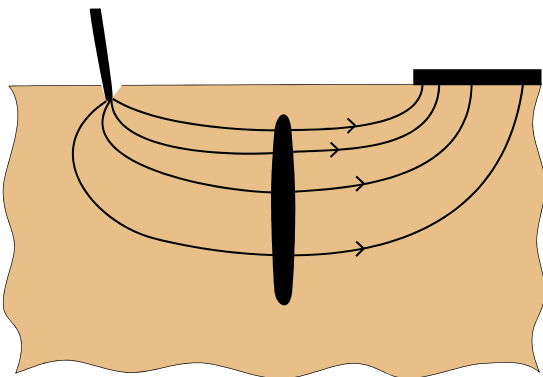
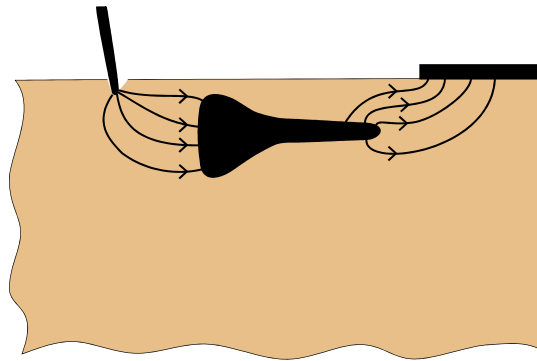
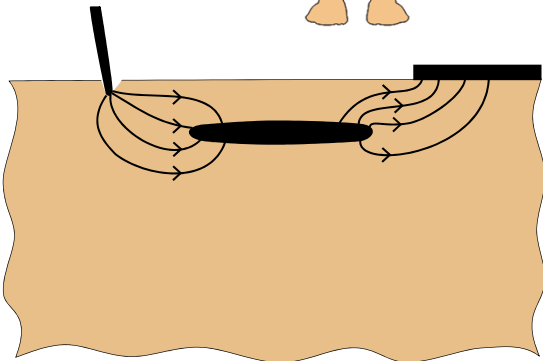
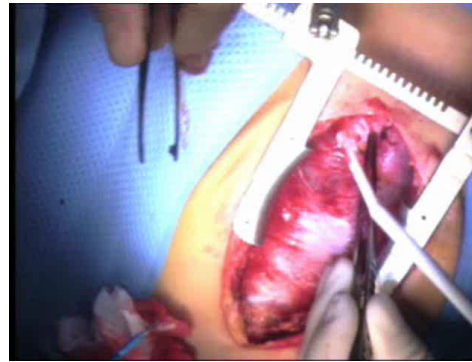
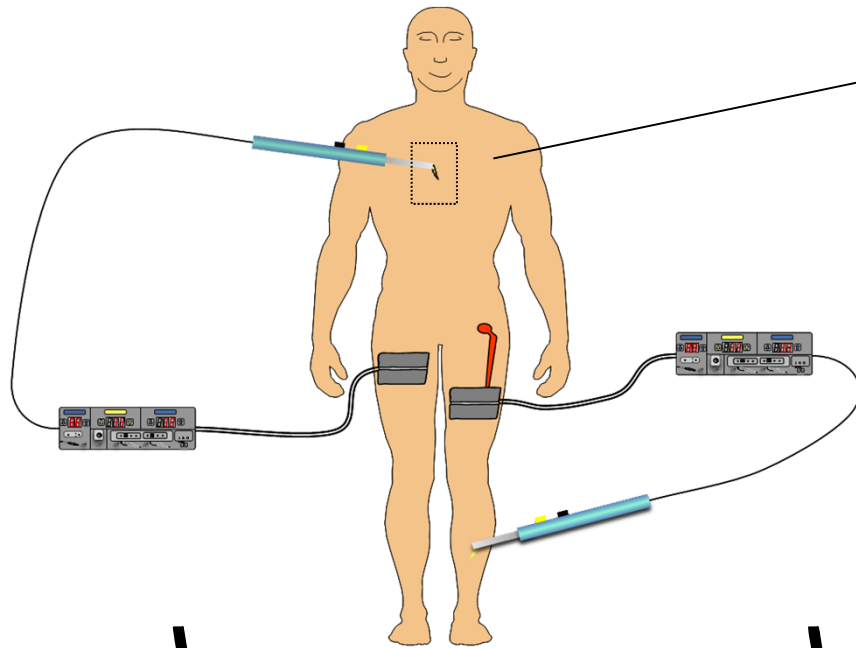


**Fig. 16.27** Fluoroptic method of temperature measurement: Spectral responses of the excitation and emission signals (a) exponential decay of the emission signal for two temperatures ( $T_1$  and  $T_2$ ) (b); where  $e$  is the base of natural logarithms, and  $\tau$  is a decay time constant (adapted from [17])

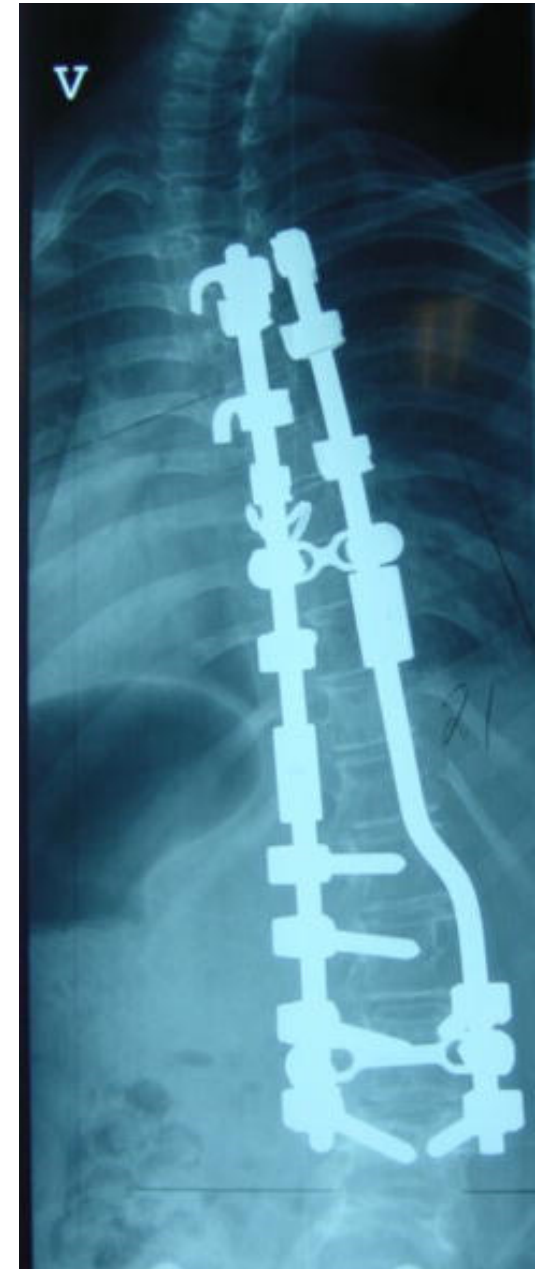
# Optiske sensorer: Interferometrisk

- Brytningsindeksen til Si er temp-avhengig
- Dette gir endret lys-vei og dermed faseforskyvning
- → Endring i intensitet i modulert signal



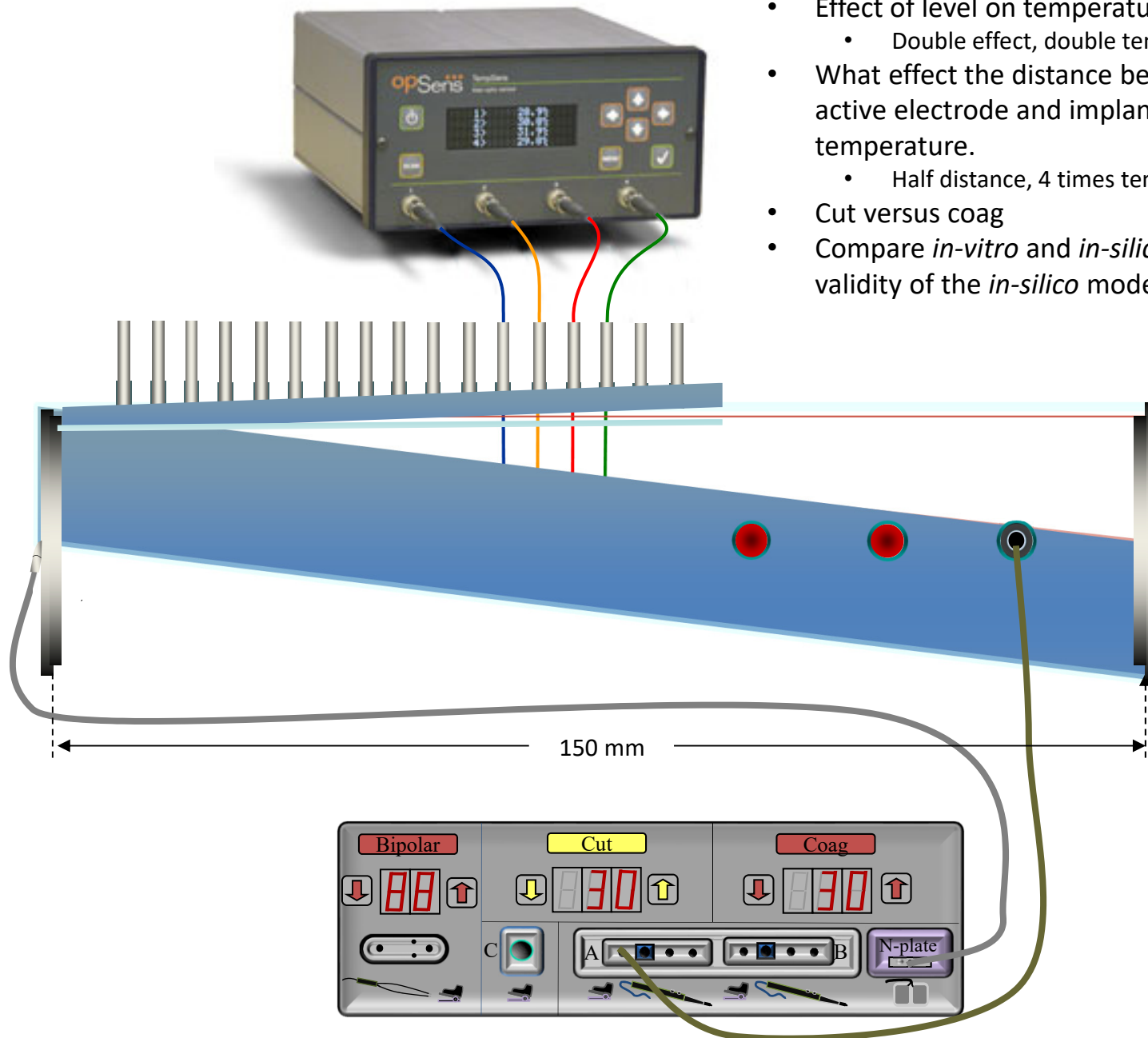


Project material from:  
Tormod Martinsen, MTV/OUS



### Some aims (short versions):

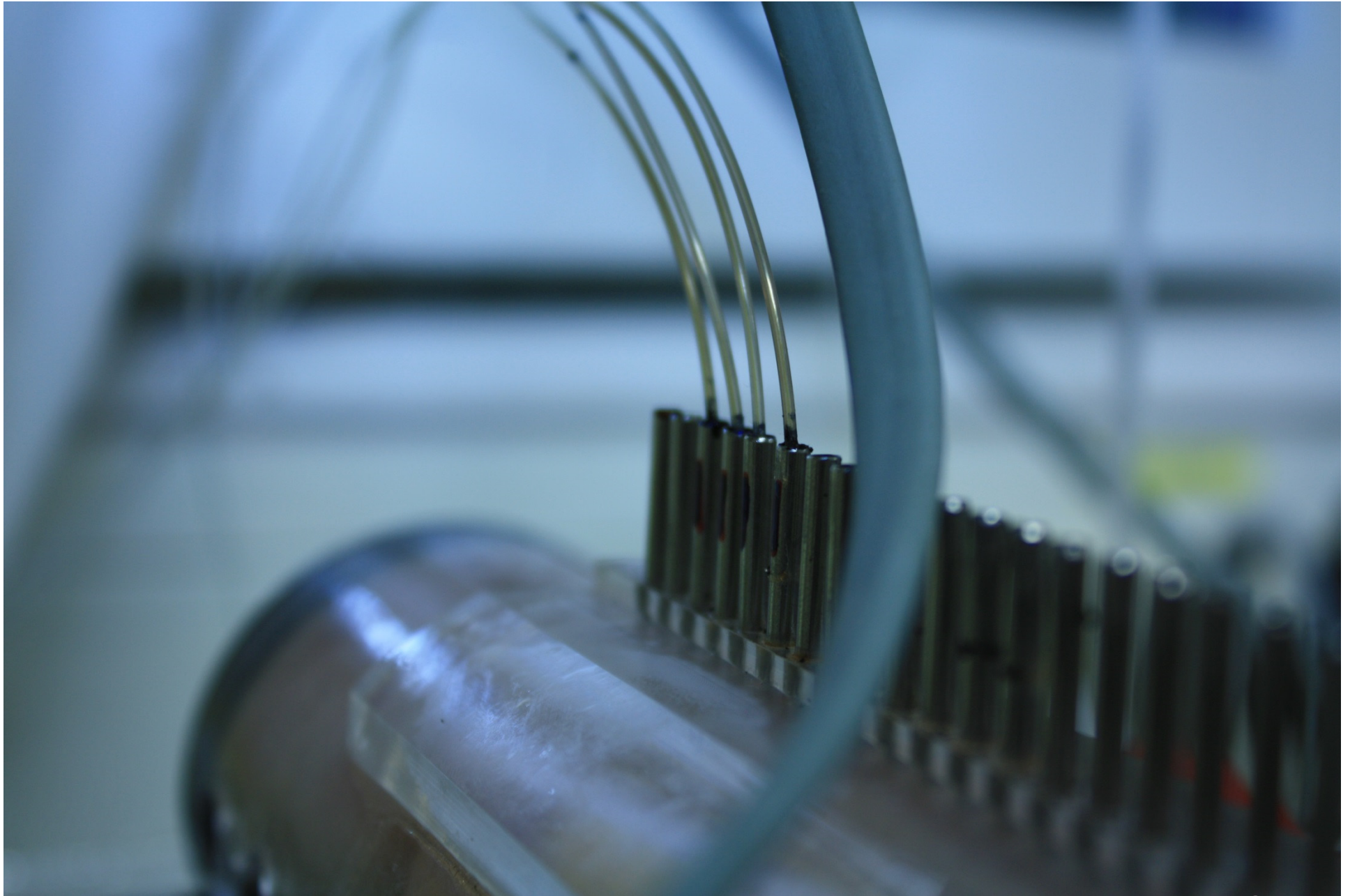
- Effect of level on temperature?
  - Double effect, double temperature?
- What effect the distance between electro-surgery active electrode and implant has on the temperature.
  - Half distance, 4 times temp?
- Cut versus coag
- Compare *in-vitro* and *in-silico* model, verify the validity of the *in-silico* model



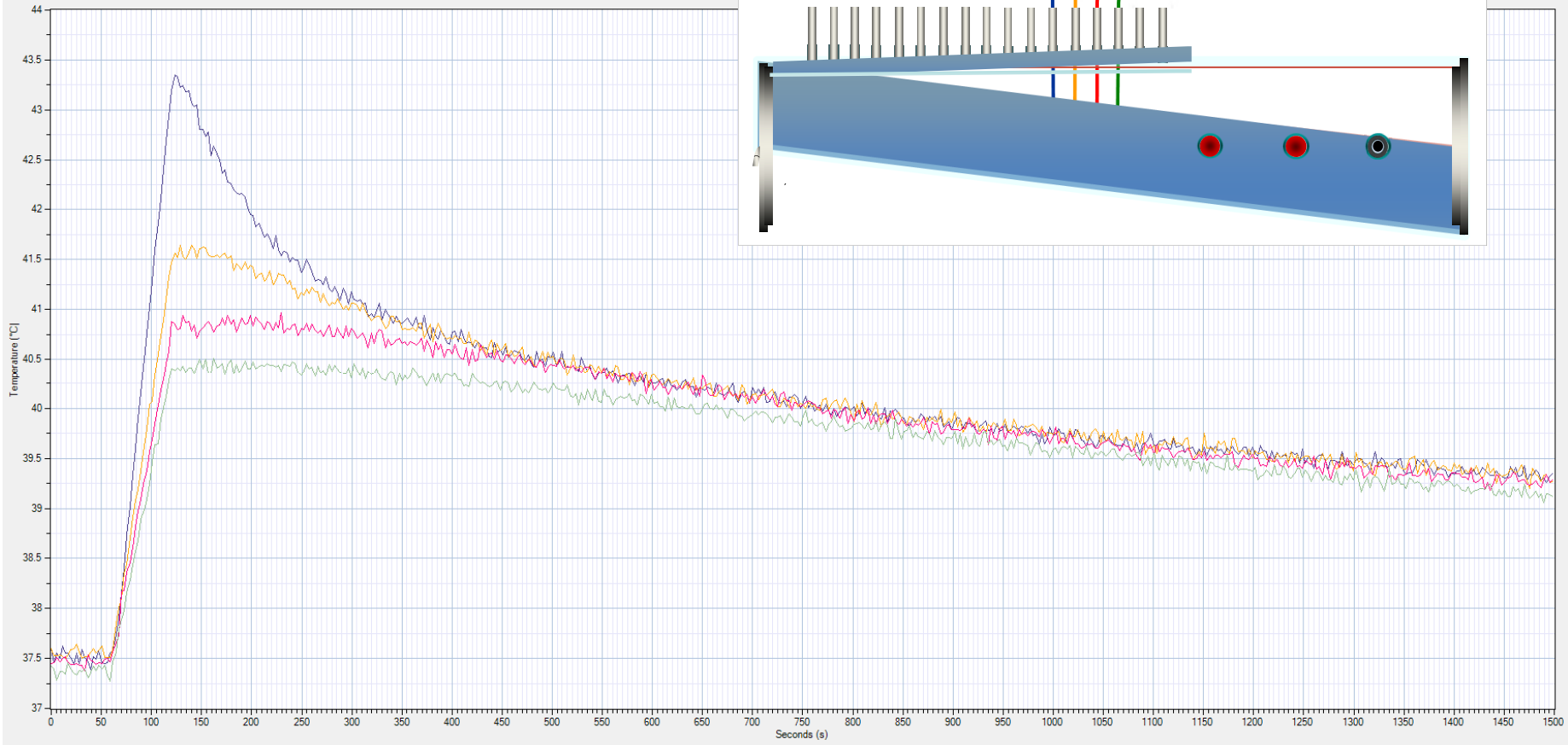
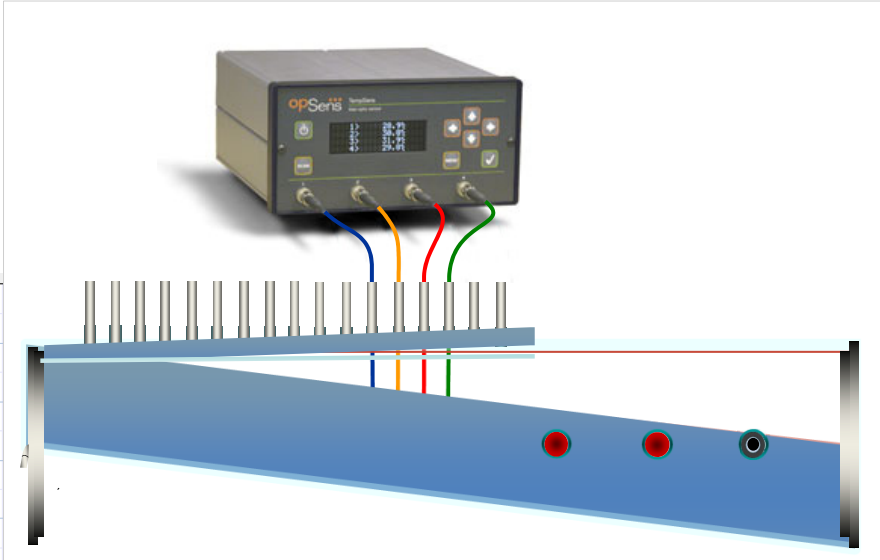




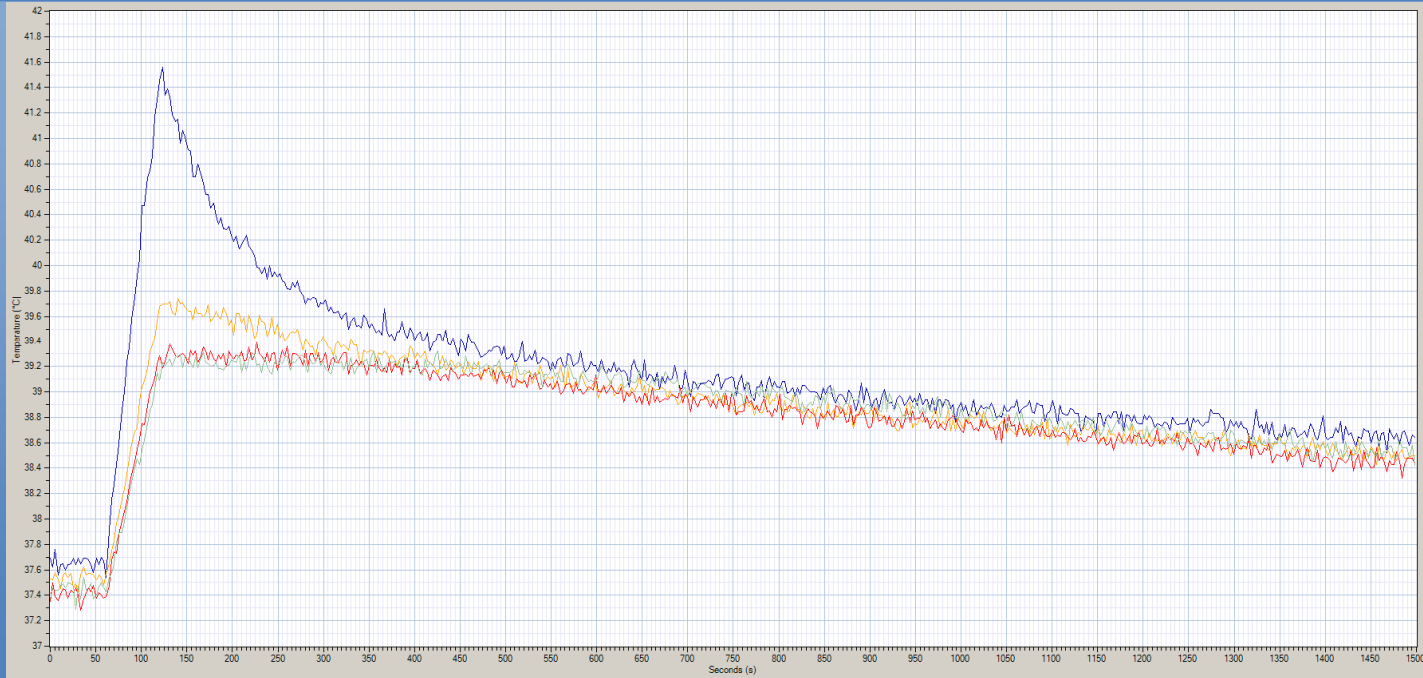




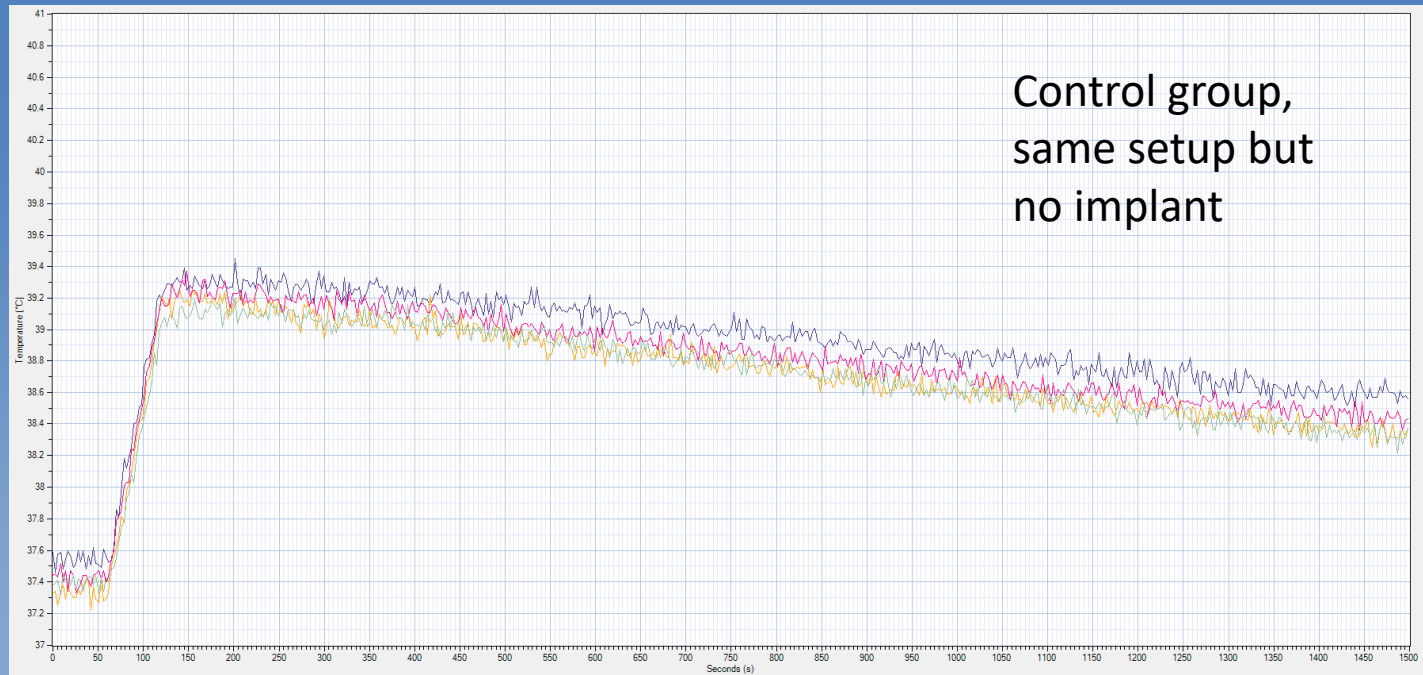
60W Coag fulgurate Position 1



M8 30W Coag  
fulgurate P2



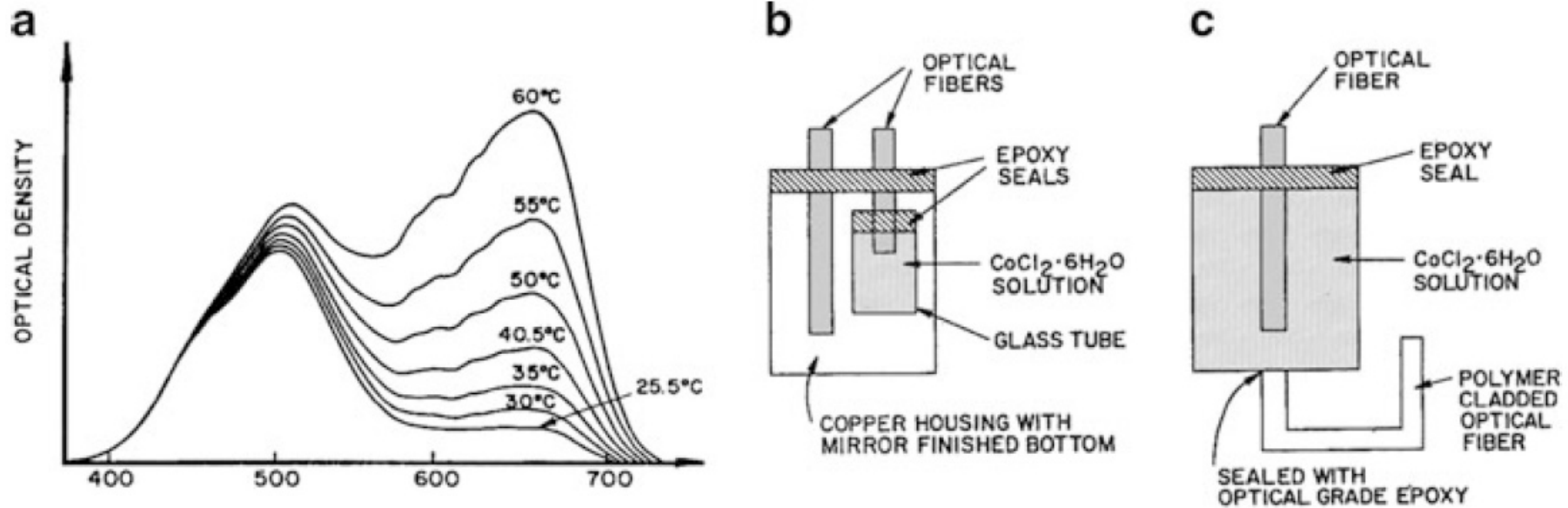
M7 30W Coag  
fulgurate P2 K1



Control group,  
same setup but  
no implant

# Optiske sensorer: Termokrom

- Temperaturavhengig spektral absorpsjon av synlig lys



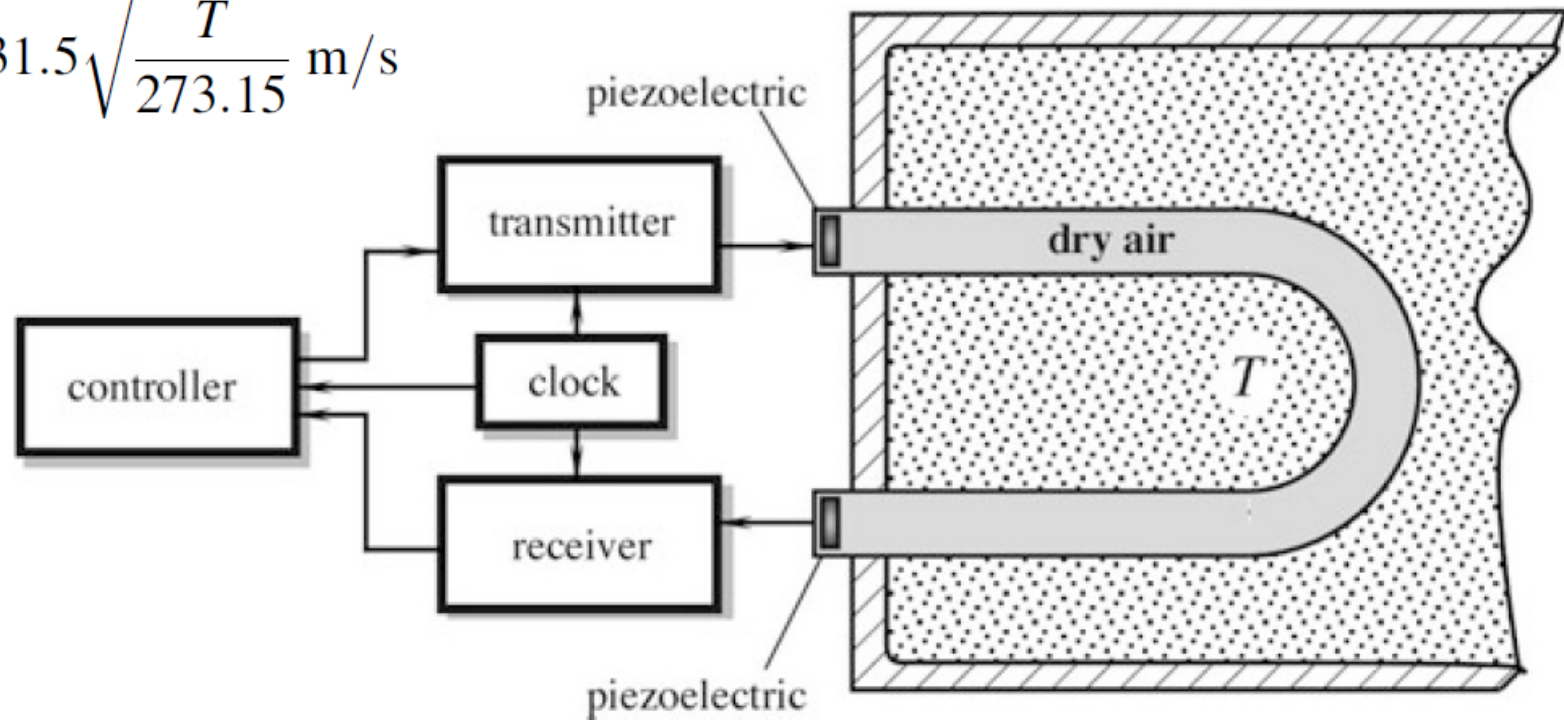
**Fig. 16.30** A thermochromic solution sensor. Absorption spectra of the cobalt chloride solution (a); reflective fiber coupling (b); and transmissive coupling (c) (from [22])



# Akustisk sensor

Tørr luft:

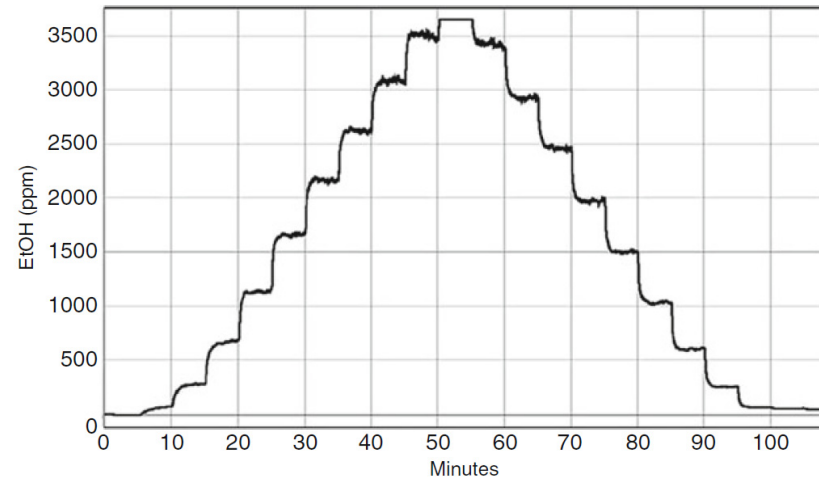
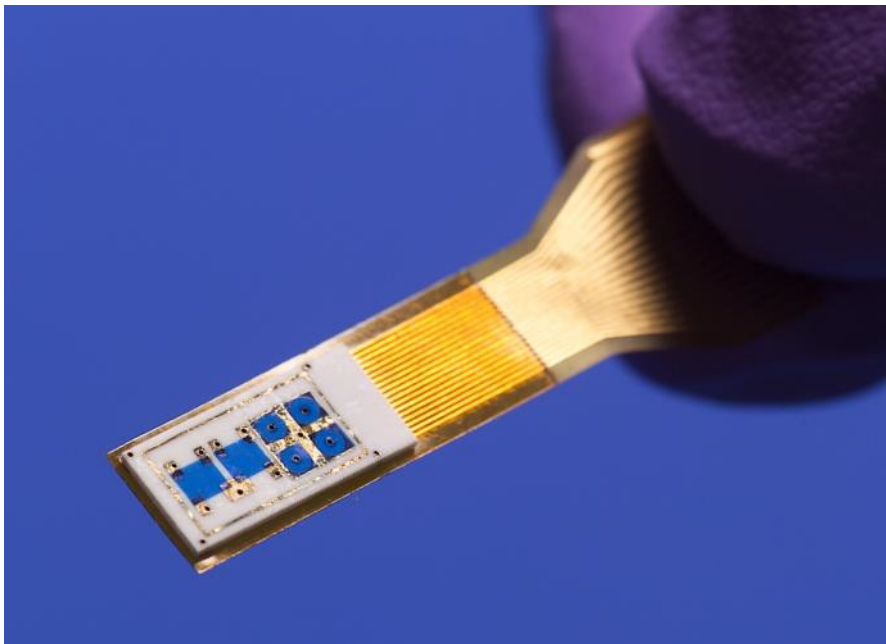
$$v \approx 331.5 \sqrt{\frac{T}{273.15}} \text{ m/s}$$



**Fig. 16.31** Acoustic thermometer with an ultrasonic detection system

# Kjemiske sensorer

- Sensitivitet (her: oppløsning) og spesifisitet
- Tre typer, basert på endring i:
  - Elektriske / elektrokjemiske egenskaper
  - Fysiske egenskaper
  - Optiske egenskaper



**Fig. 17.2** Metal-oxide-semiconductor-based sensor response to increasing and decreasing concentrations of ethanol

# Eksempel på spesifisitet (Volatile Organic Compound – VOC)

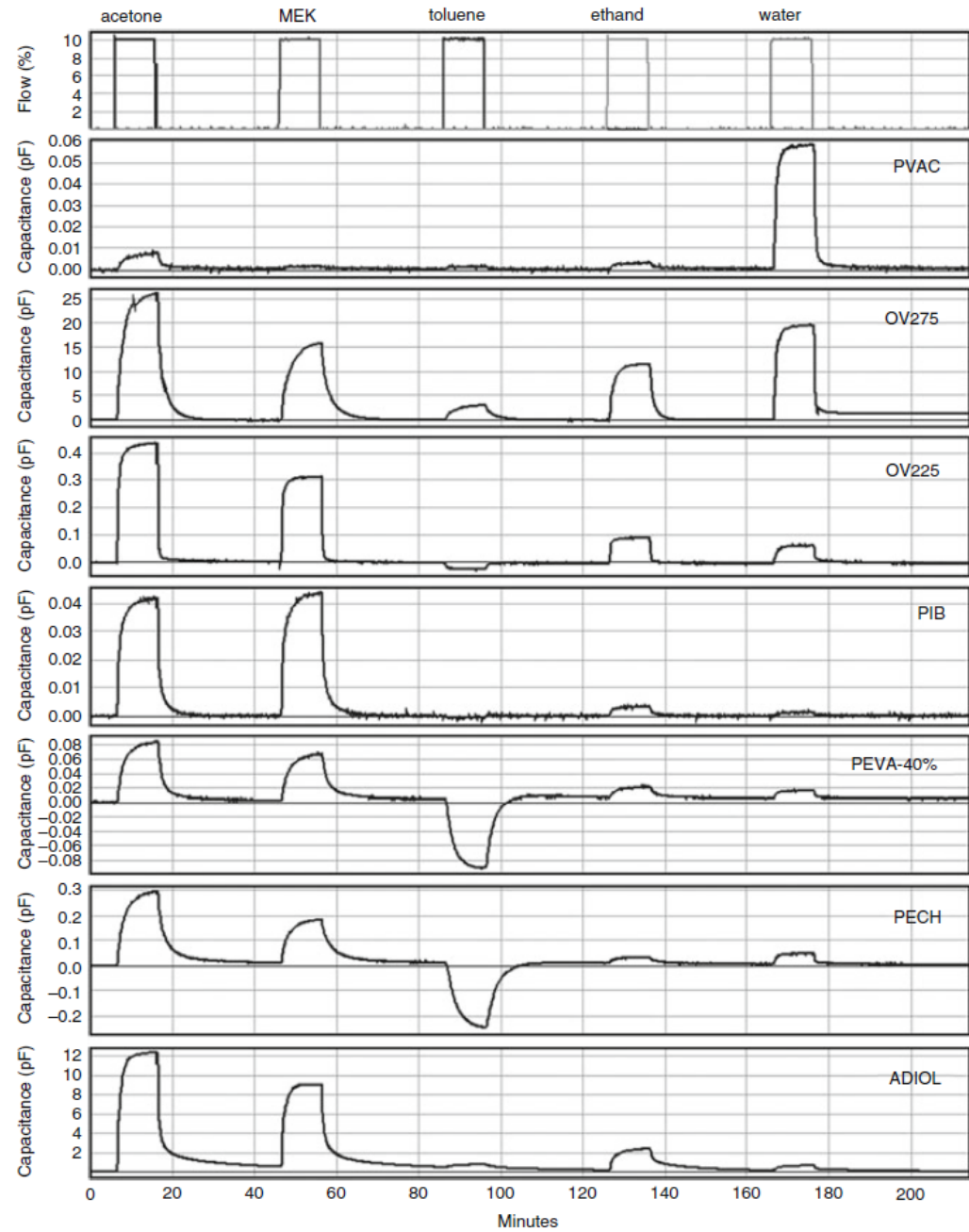
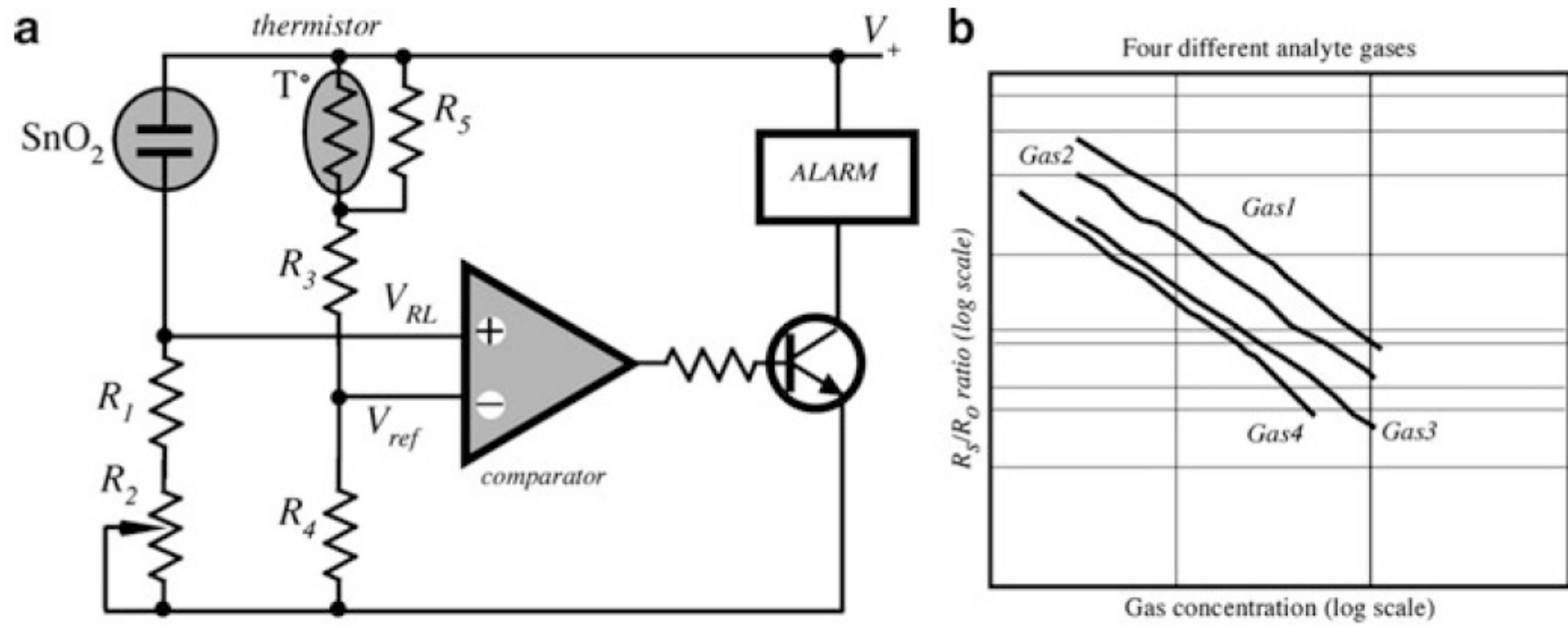
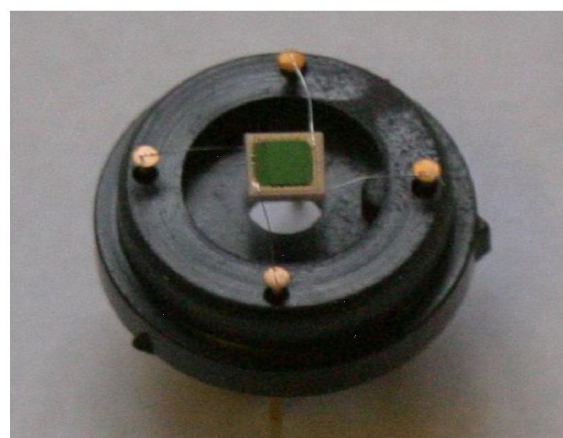


Fig. 17.3 Response of a capacitive VOC sensor array containing seven differently absorbing polymer-coated chemicapacitors to pulses of acetone, methyl ethyl ketone, toluene, ethanol, and water at 25°C



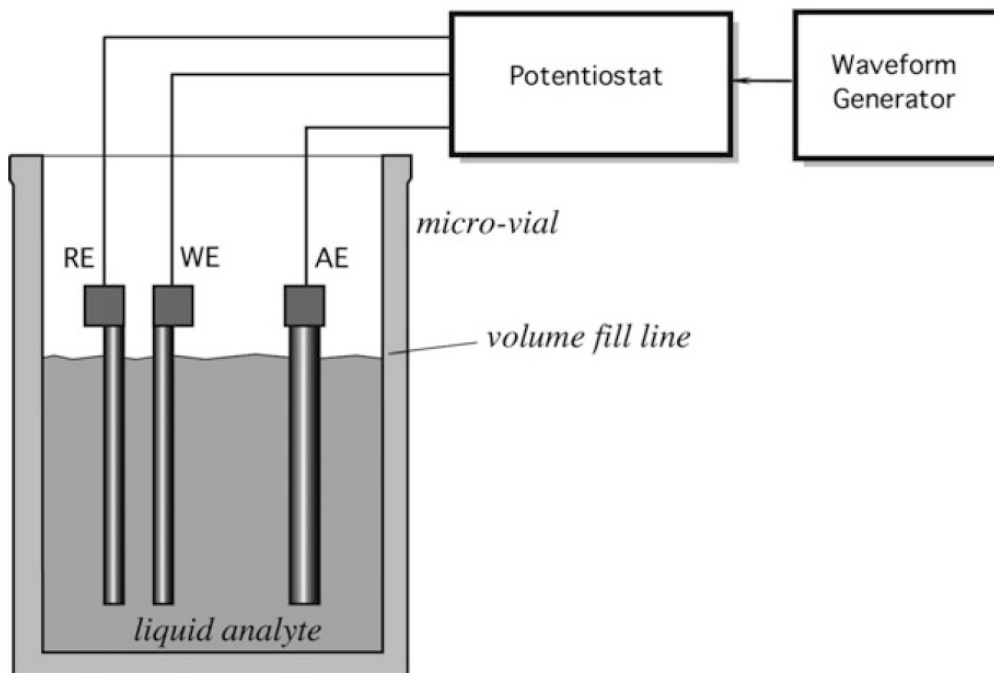
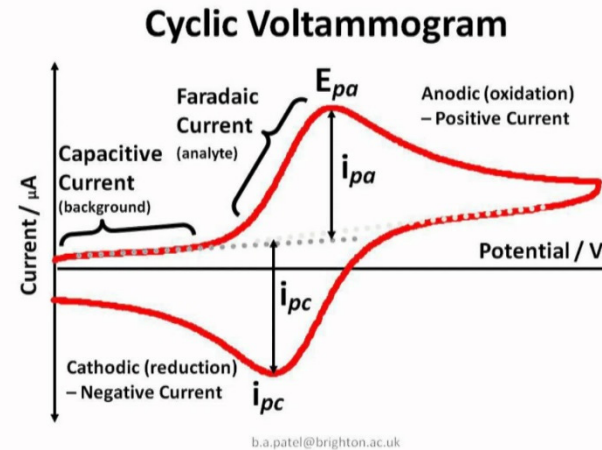
# Metalloksyd-sensor

- Resistansen endres ved endrede kjemiske omgivelser (gass)
- NTC termistor for å kompensere for temp-endringer



**Fig. 17.4**  $\text{SnO}_2$  Wheatstone bridge circuit (a) used for metal-oxide sensors and responses to different gases (b)

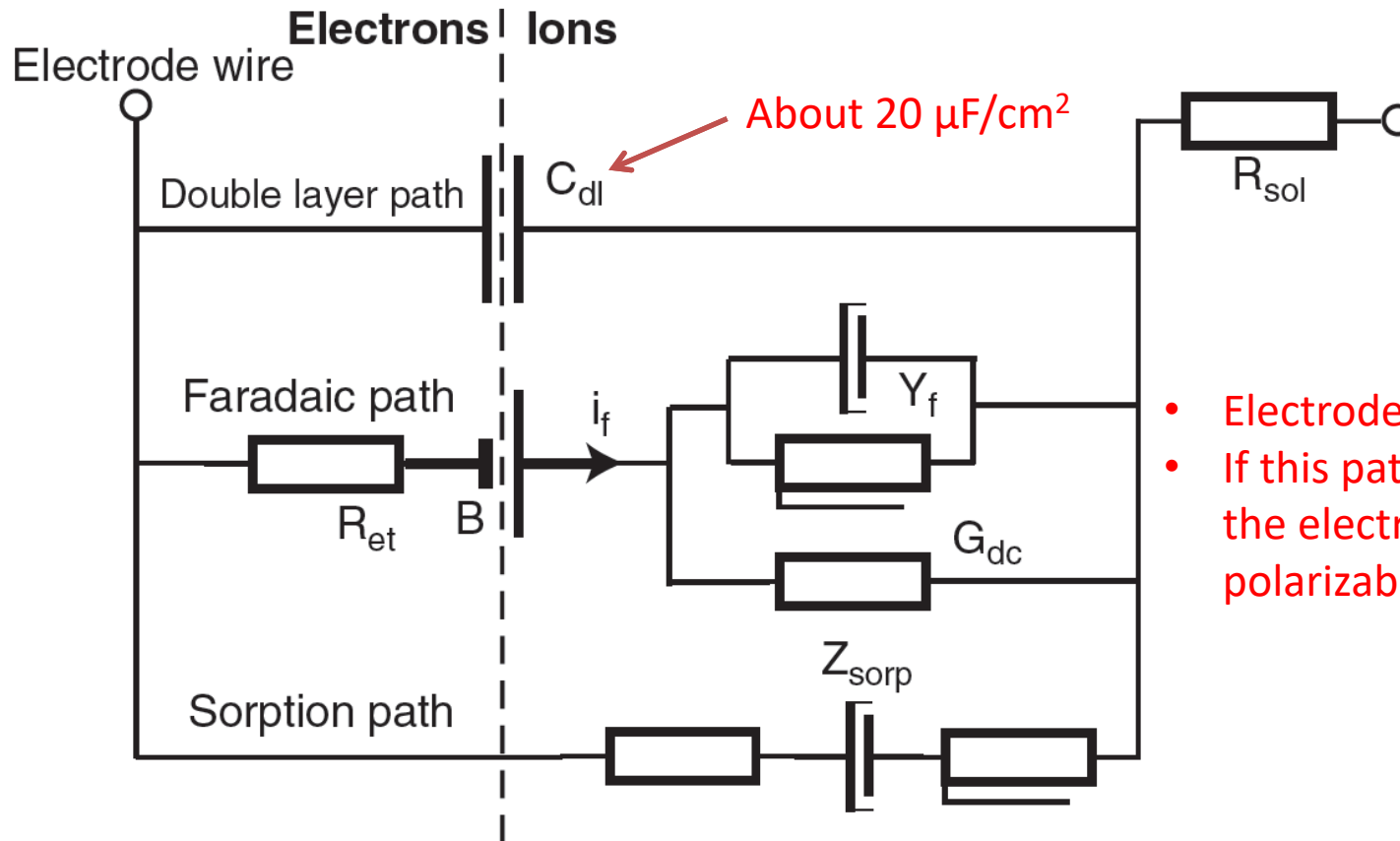
# Elektrokjemiske sensorer



- Måler spenning, strøm eller konduktans
- Working, Auxiliary og Return electrodes
- To-elektrode-systemer brukes også
- Potensiometriske sensorer måler halvcellepotensial
- Amperometriske sensorer måler Faradaisk strøm pga redox-prosesser

Fig. 17.5 Electrochemical-sensor electrode set

# Electrode polarization impedance



- Electrode reactions
- If this path is missing, the electrode is polarizable

- Adsorption/desorption of species at the electrode surface
- No electron exchange
- May dominate for noble metals

# Kapasitive sensorer

- Absorberende polymer som dielektrikum
- F.eks. hygrometer

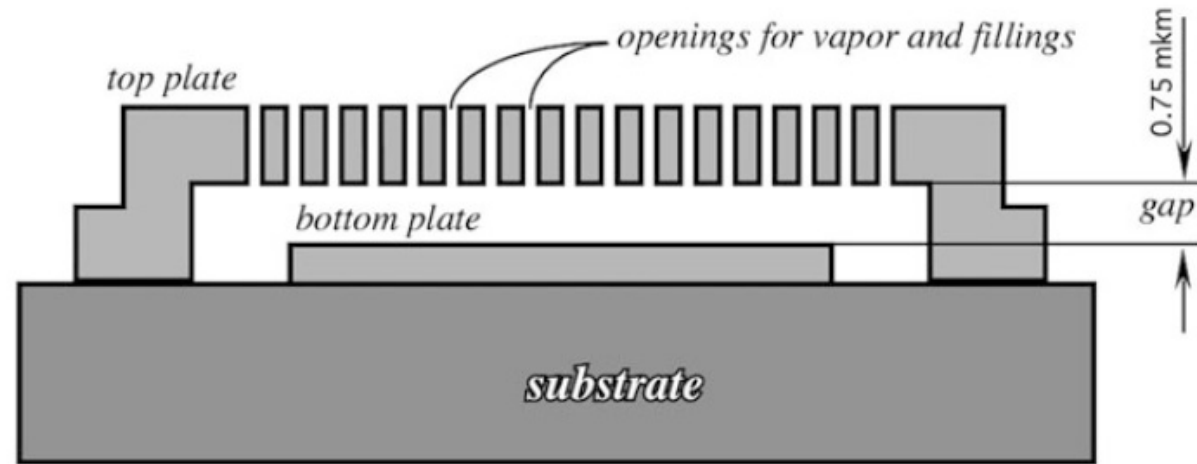
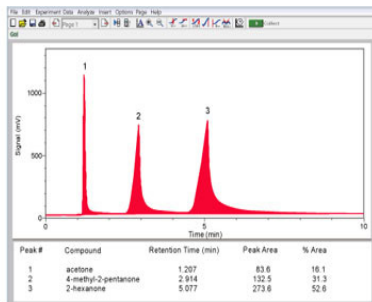


Fig. 17.9 Cross-section diagram of the parallel-plate capacitor showing the 0.75 μm gap

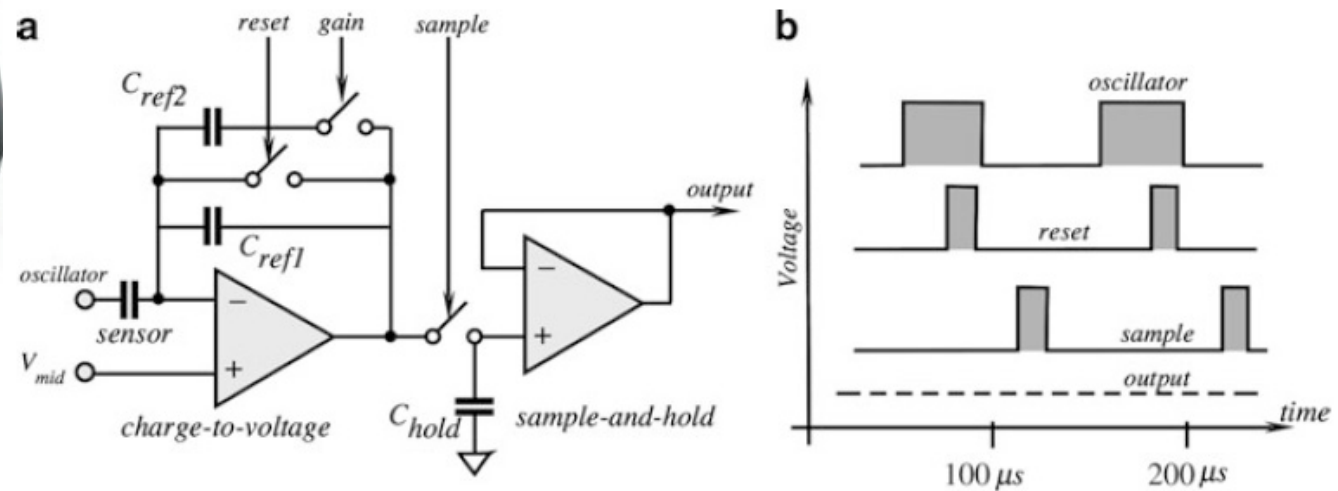


Fig. 17.10 Capacitance measurement circuit (a) and timing diagrams (b)

# Fotoioniserende detektor



- UV-lys ioniserer molekyler  
→ strøm i E-felt
- Lysets energi bestemmer  
hvilke gasser som kan  
ioniseres

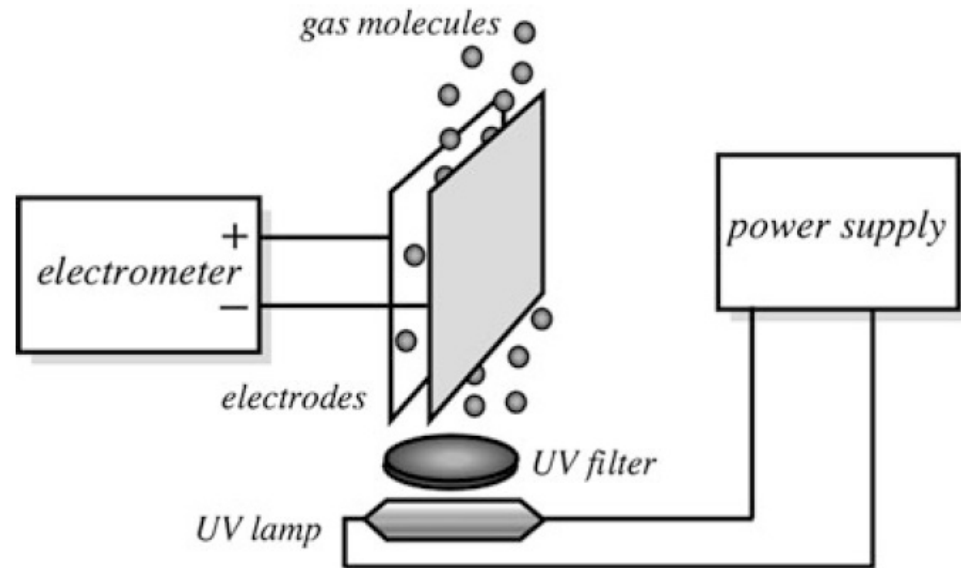


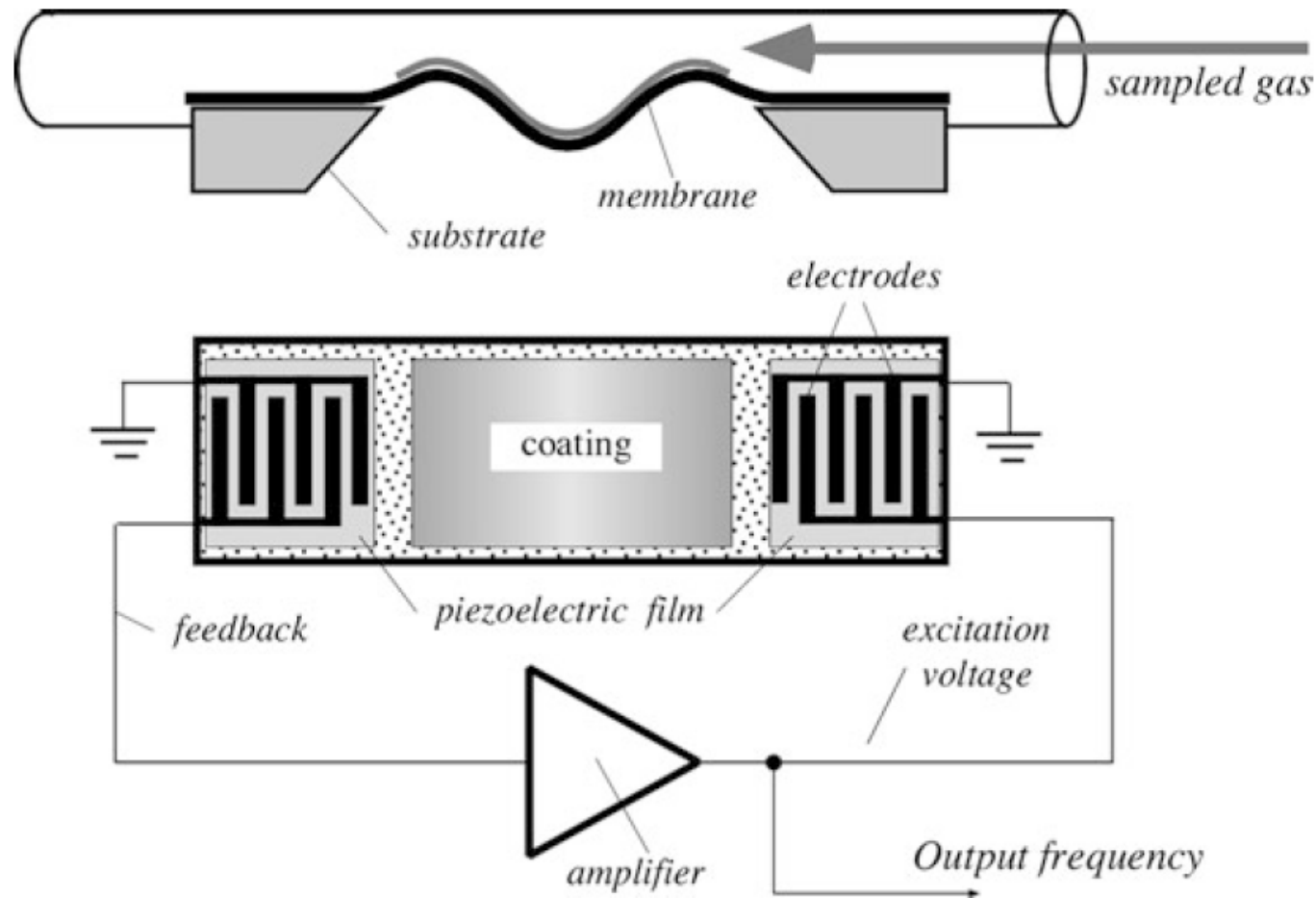
Fig. 17.13 Concept of PID detector

# Fysikalske transdusere

*(ingen kjemisk reaksjon)*

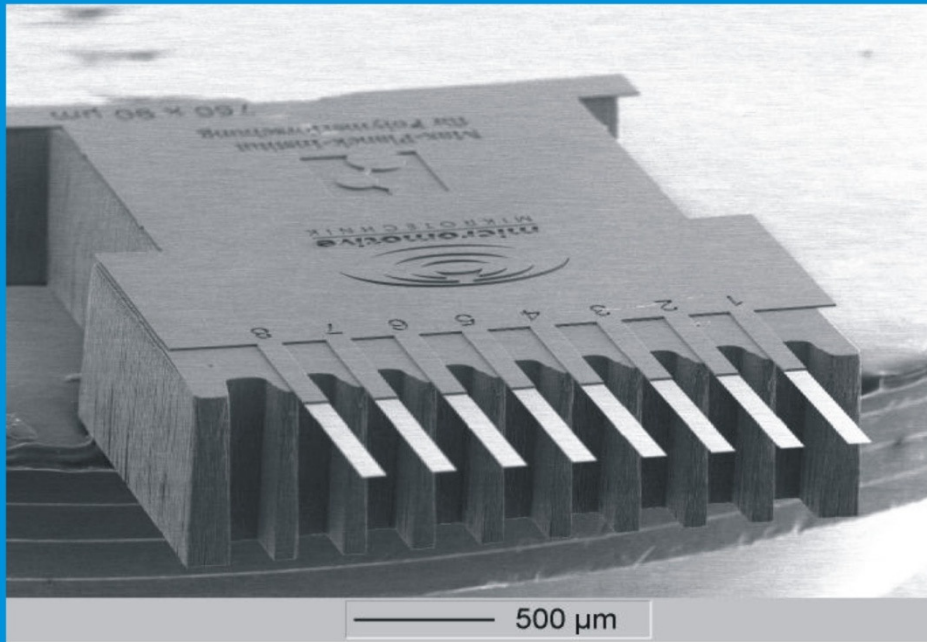
- Prøvematerialet absorberer det aktuelle stoffet.
- Akustisk sensor. Frekvensen reduseres når massen øker. Resonans eller forsinkelseslinje.
- Mikrokantilever (vektstang). Bøyes pga endrede overflatespenninger (ikke pga vekt).
- Ionemobilitetsspektrometer.
- Termiske sensorer. Eksoterme eller endoterme reaksjoner.

# Akustisk sensor

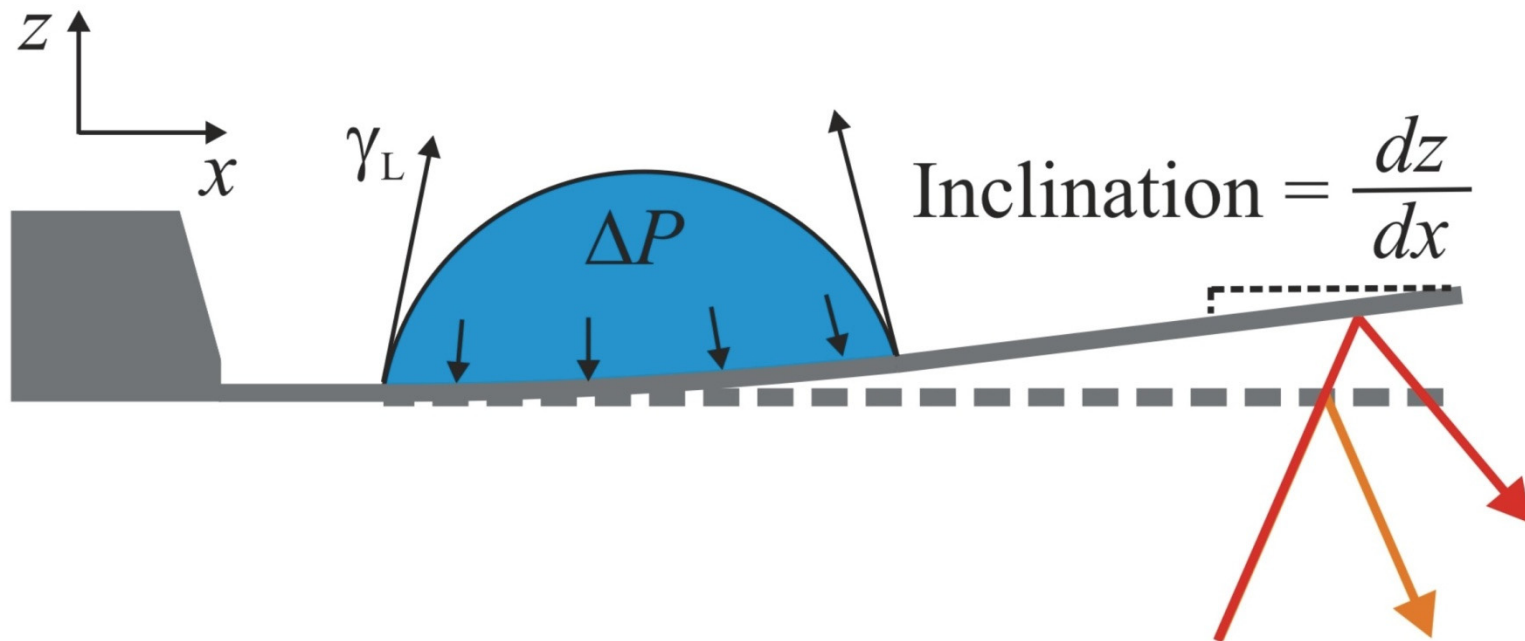


**Fig. 17.15** Flexural plate SAW gas sensor (deflection of the membrane is exaggerated for clarity)





# Mikrokantilever



# Mobilitets-spektrometer

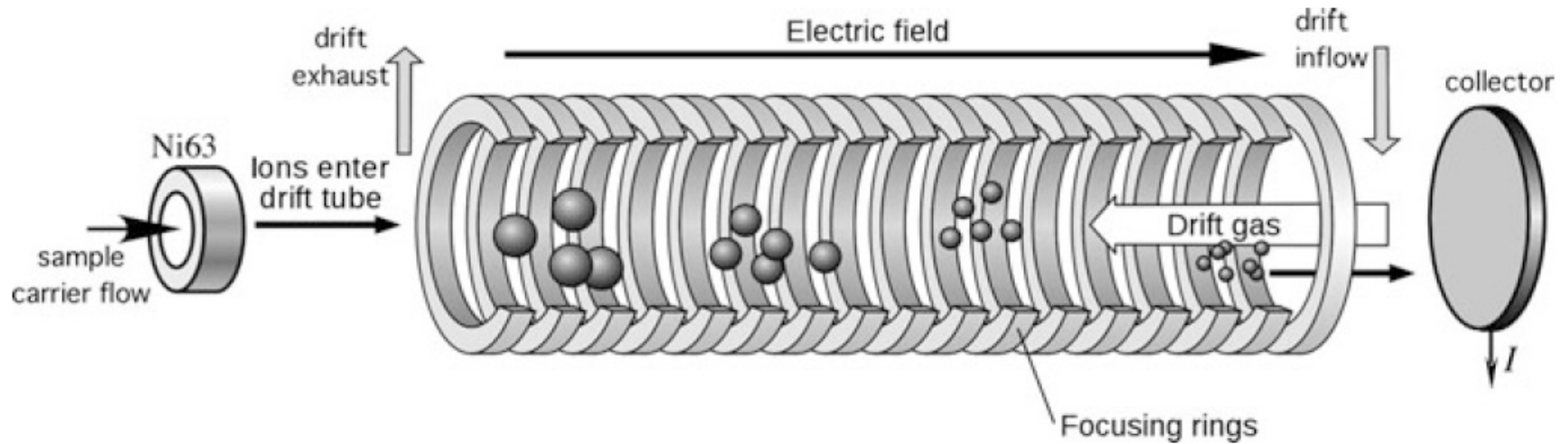


Fig. 17.18 Principle of ion mobility spectrometry

# Optiske transdusere

- Absorpsjon av forskjellige bølgelengder (ofte IR)
- Refleksjon (fiberoptisk)



# Biosensor

- Ofte enzymer som virker som katalysatorer.
- Det kjemiske produktet registreres med en annen metode.

