

**GEO4250**  
**Reservoir Geology**

Basic Well Log Analysis

*Determination of Saturation*

# Reminder

$$N_p = \phi_e S_{hc} hAr$$

$$S_w = \sqrt[n]{\frac{FR_w}{R_t}} = \sqrt[n]{\frac{R_o}{R_t}}$$

$$S_w = 1 - S_{hc}$$

$$\phi_s = \left( \frac{\Delta t_{\log} - \Delta t_{\text{matrix}}}{\Delta t_f - \Delta t_{\text{matrix}}} \right) \quad \text{Sonic Porosity}$$

$$\phi_{\text{den}} = \frac{\rho_{\text{matrix}} - \rho_b}{\rho_{\text{matrix}} - \rho_f} \quad \text{Density Porosity}$$

$\phi_n$  from log

$$\phi_e = \phi_t \times (1 - V_{sh}) \quad \text{Effective Porosity}$$

$$F = \frac{R_o}{R_w} = \frac{a}{\phi^m}$$

# Reminder

- Determined  $R_w$  from the Spontaneous Potential
- Determined  $\phi_t$  and  $\phi_e$  from porosity and gamma ray logs
- The only parameter we lack now is the true resistivity of the formation

# Resistivity

- The resistivity (**specific resistance**) of a substance is the resistance between opposite faces of a unit cube of that substance at a specific temperature
- Symbol  $R$ , measured in  $\Omega \cdot m$  (ohm·m<sup>2</sup>/m)

$$R = \frac{r \times A}{L}$$

- With  $r$  = resistance in ohms;  $A$  = area in square meters;  $L$  = length in meters
- Resistivity is a basic measurement of a reservoir's fluid saturation and is a function of porosity, type of fluid, amount of fluid and type of rock
- Usually between 0.2 and 1000 ohm·m

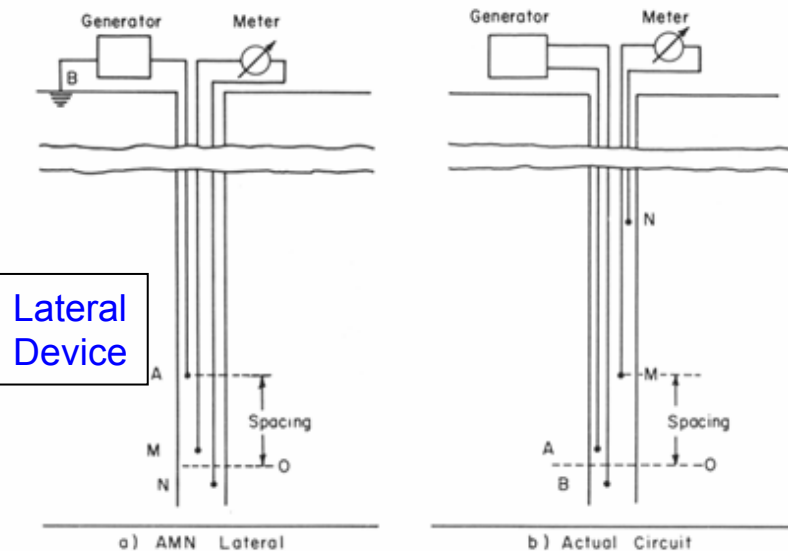
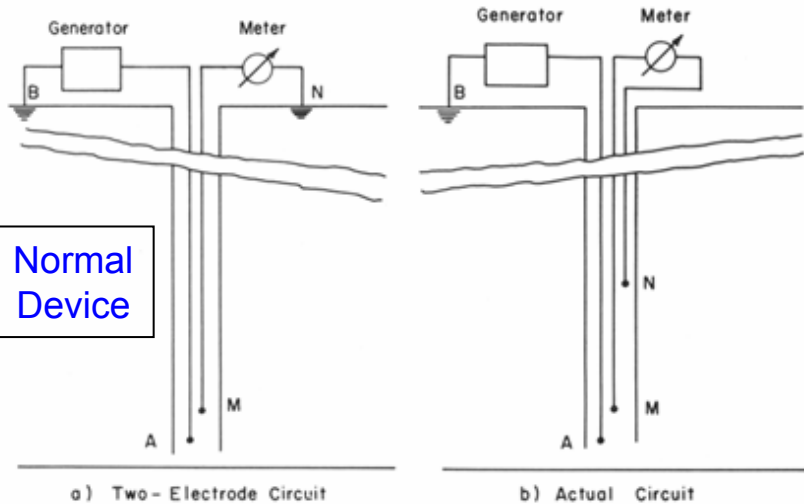
# Resistivity

- Dependent on:
  - Presence of Formation water / Hydrocarbons
  - Salinity of Formation water
  - Temperature of Formation water
  - Volume of water-saturated pore space
  - Geometry of the pore space
  - Morphology and species of clay minerals

# Tools

- Conventional Electrical logs
  - First developed before 1950
    - Normal devices
      - Short Normal (SN)
      - Long Normal (LN)
    - Lateral devices
      - Laterologs (LL, e.g. LL3, LL7, LL8, LLD, LLS, SFL)
- Induction logging
  - First developed after 1950
    - Induction devices
      - 6FF40 (combined tool: Induction, Normal and SP, 1960's)
      - DIL-LL8 (improved induction-normal combination)
      - Induction SFL
      - DIL-SFL
      - Phasor Induction SFL
      - Other abbreviations: ILD, ILM, ILS, RD, RM, RS, RT

# Conventional Electrical Logging



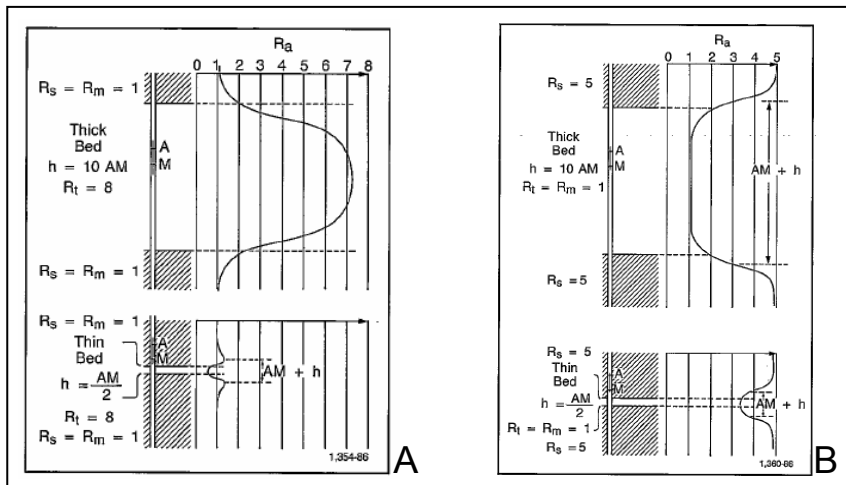
- Current of constant intensity between A and B
- Resultant potential difference measured between M and N
- The larger the 'spacing', the deeper the measurement

# Conventional Electrical Logging

## Normal and Lateral Curves

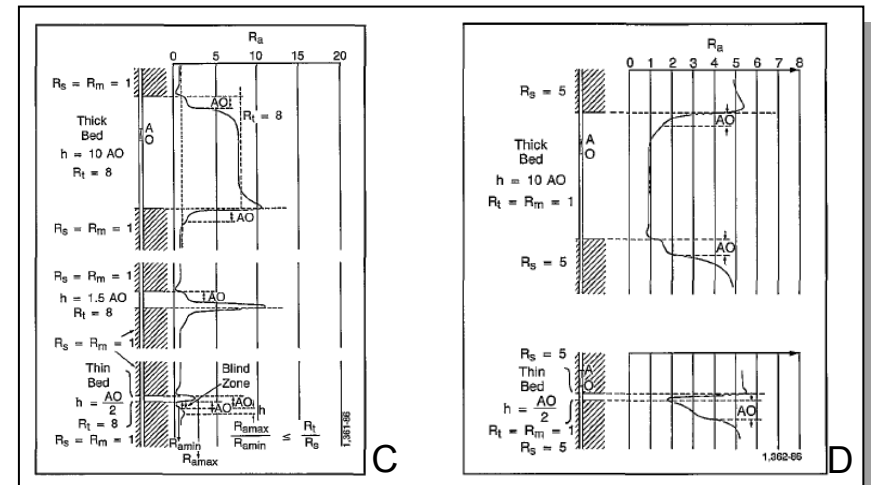
### Normal Device

- A: Beds more resistive than surrounding beds
- B: Beds less resistive than surrounding beds



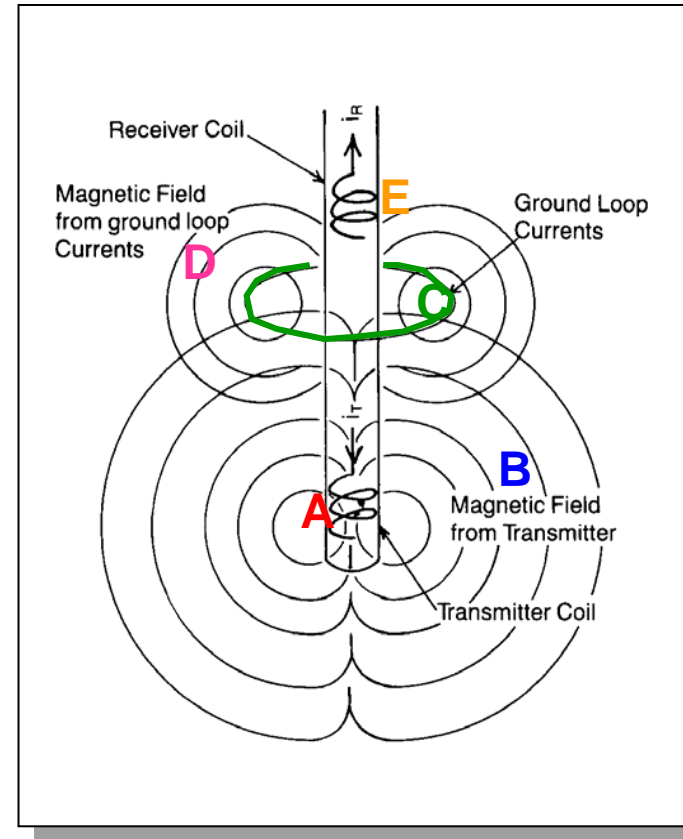
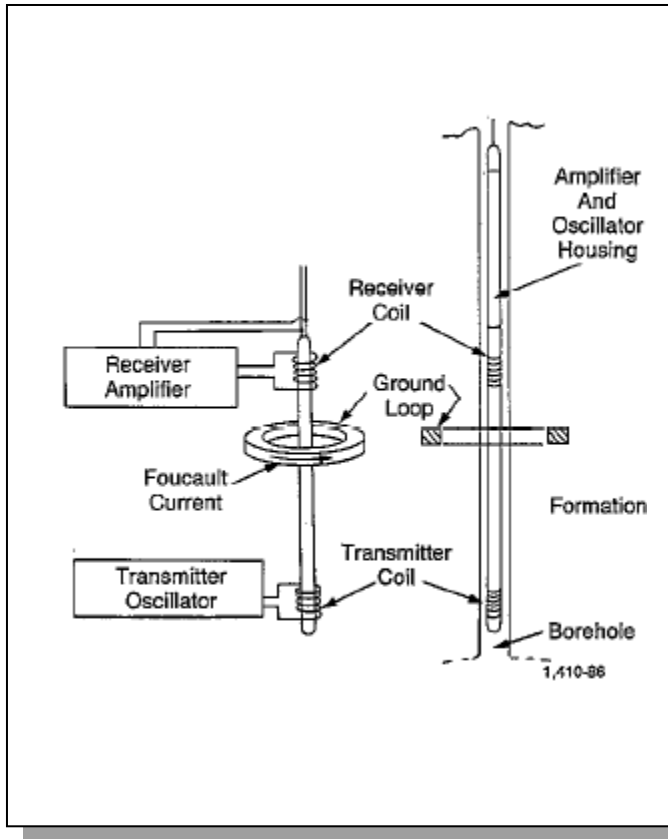
### Lateral Device

- C: Beds more resistive than surrounding beds
- D: Beds less resistive than surrounding beds





# Induction Logging

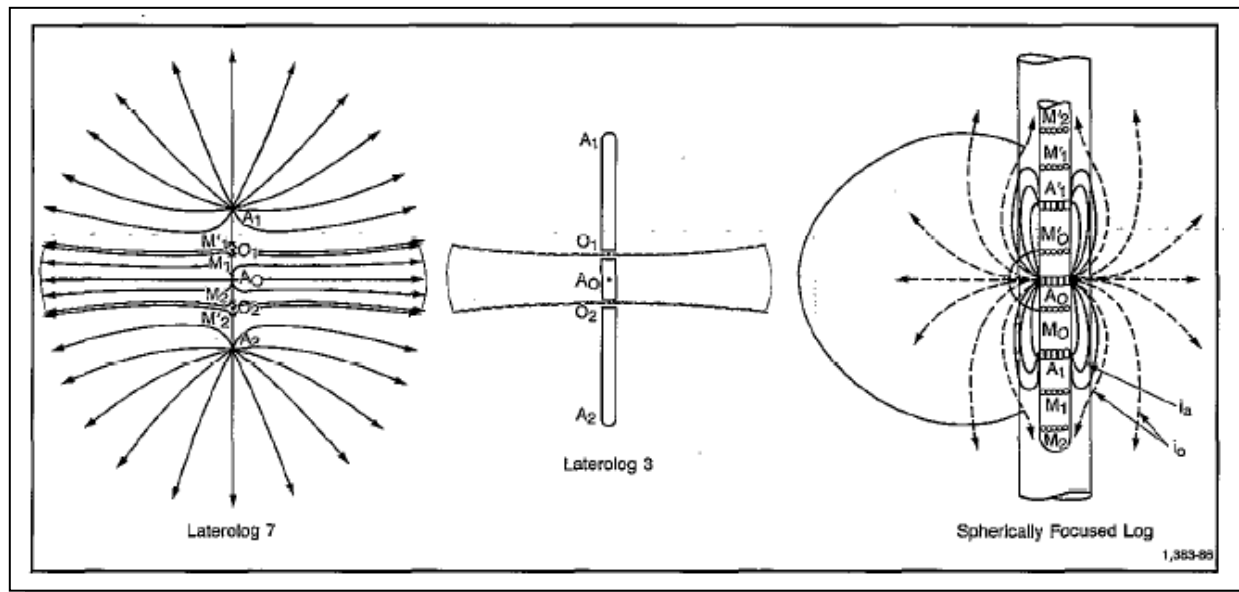


- High frequency, alternating current of constant intensity is sent through a transmitter coil (A)
- The alternating magnetic field (B) created, induces currents in the formation surrounding the borehole (C)
- These currents flow in circular ground loops coaxial with the transmitter coil and create, in turn, a magnetic field (D) that induces a current in the receiver coil (E)

# Resistivity Logging

## *Focusing*

- Minimization of borehole and adjacent formation affects
- Focusing currents to control the path taken by the measure current



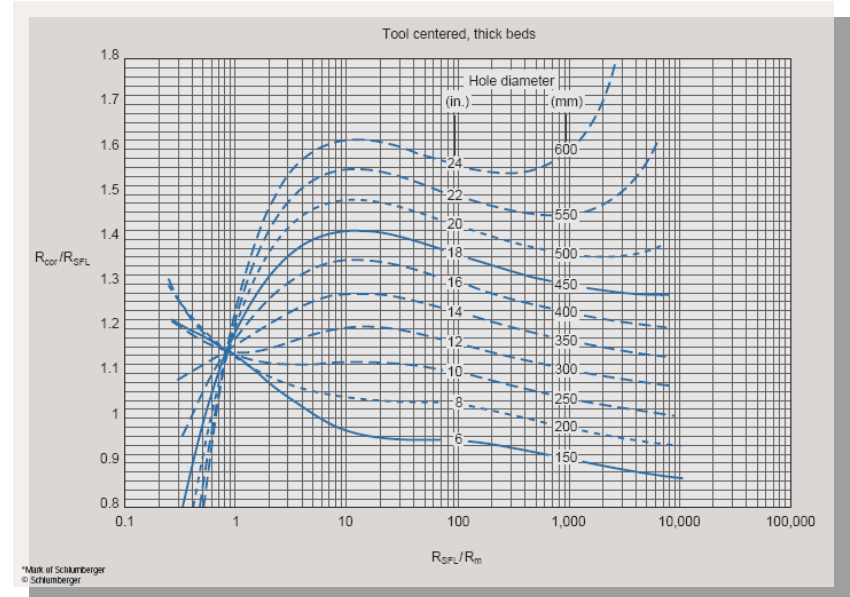
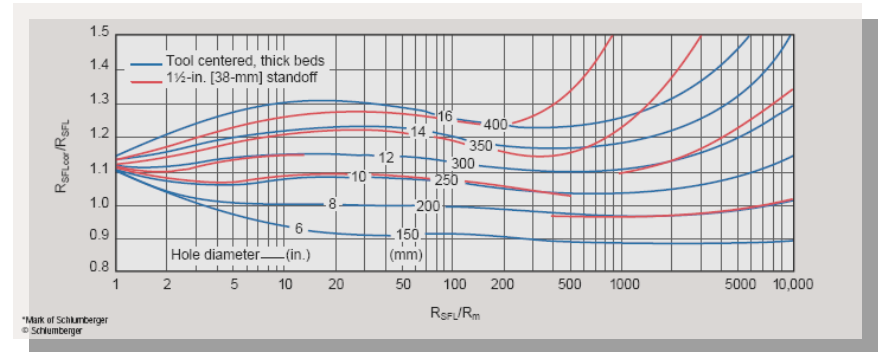
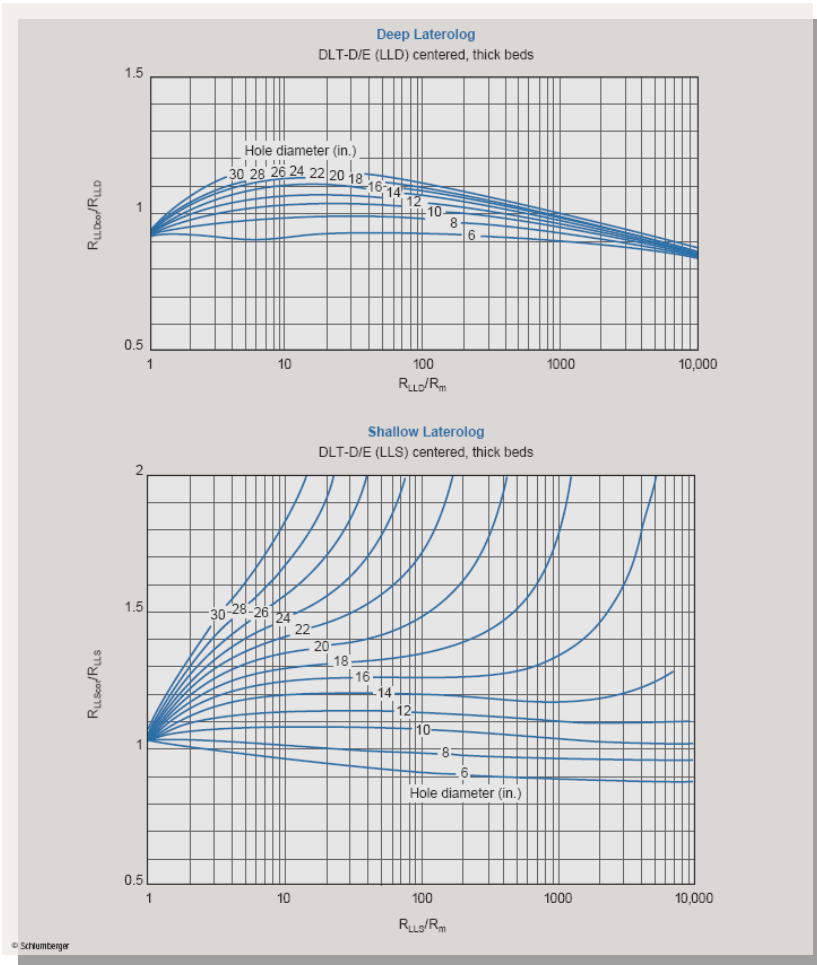
# Resistivity Logging

## *Influence of well bore variables and log correction*

- Resistivity measurements are influenced by:
  - Borehole mud
  - Adjacent beds
  - Invaded zone
- Readings must be corrected, always in the following way:
  - Borehole effect
  - Adjacent bed effect
  - Invasion correction

# Resistivity Logging

## Corrections - Borehole Effect



# Resistivity Logging

## Corrections - Adjacent Bed Effect

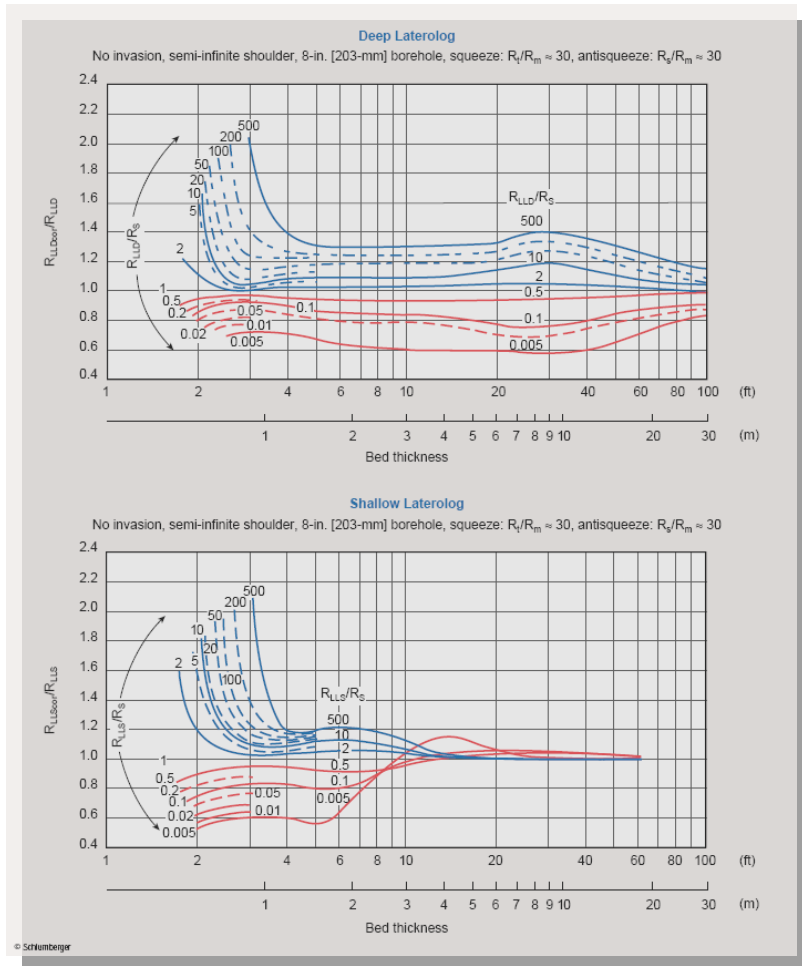


Chart Rcor-10 corrects the Dual Laterolog (LLD and LLS) for bed thickness.

To use, laterolog readings should first be corrected for borehole effects (see Charts Rcor-2b and -2c). Then, enter Chart Rcor-10 with the bed thickness and proceed upward to the proper  $R_{LL}/R_s$  ratio (apparent laterolog reading corrected for borehole/adjacent-bed resistivity) curve. Read the ratio of the corrected laterolog value ( $R_{LLcor}$ ) to the apparent laterolog value ( $R_{LL}$ ) in ordinate.

*Example:*  $R_{LLD} = 4.2$  ohm-m

$R_{LLS} = 3.0$  ohm-m

$R_s = 30$  ohm-m

Bed thickness = 6 ft

Given  $\frac{R_{LLD}}{R_s} = \frac{4.2}{30} = 0.14$

$\frac{R_{LLS}}{R_s} = \frac{3.0}{30} = 0.10$

Therefore,  $\frac{R_{LLDcor}}{R_{LLD}} = 0.88$

$\frac{R_{LLScor}}{R_{LLS}} = 0.80$

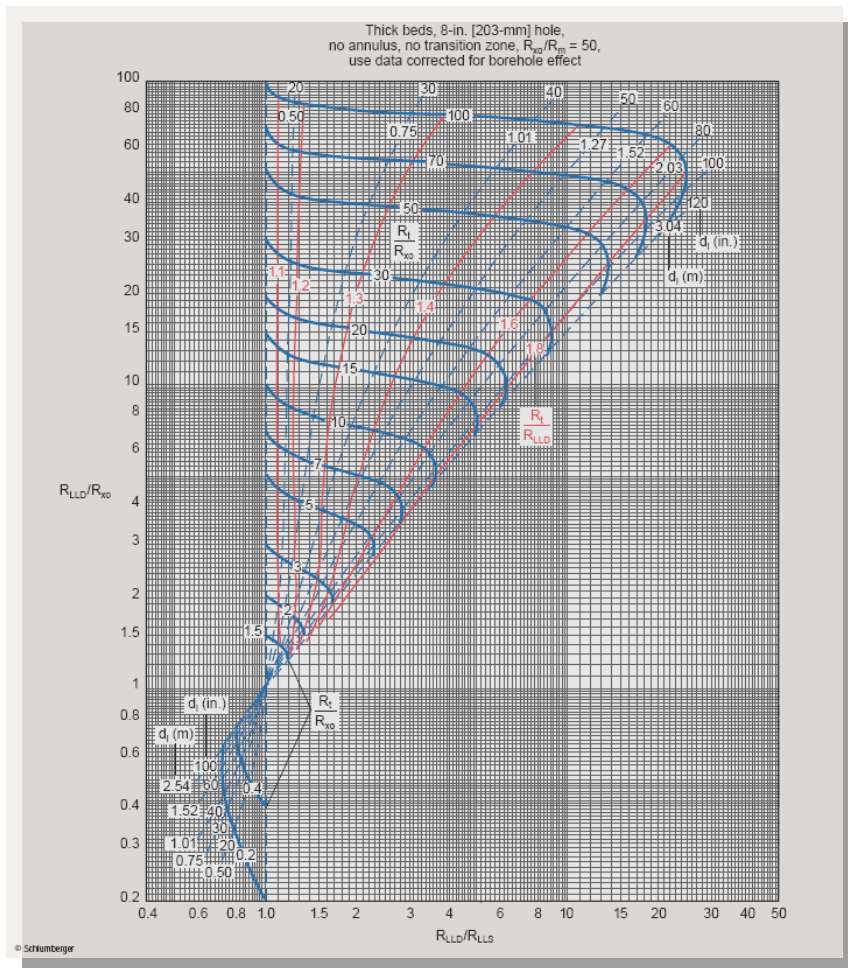
and  $R_{LLDcor} = 3.7$  ohm-m

$R_{LLScor} = 2.4$  ohm-m

# Resistivity Logging

## Invasion Correction

### 'Tornado' or 'Butterfly' Chart



The invasion correction charts, sometimes referred to as “tornado” or “butterfly” charts, of the next several pages (labeled Rint-) are used to define the depth of invasion  $d_i$ , the  $R_{xo}/R_t$  ratio and the true resistivity  $R_t$ . All assume a step-contact profile of invasion and that all resistivity measurements have been corrected, where necessary, for borehole effect and bed thickness using the appropriate  $R_{cor}$ -chart, prior to entry.

To use any of these charts, enter the abscissa and ordinate with the required resistivity ratios. The point of intersection defines  $d_i$ ,  $R_{xo}/R_t$  and  $R_t$  as a function of one resistivity measurement.

#### Saturation determination in clean formations

Either of the chart-derived values of  $R_t$  and  $R_{xo}/R_t$  can be used to find values for  $S_w$ . One value, which is designated as  $S_{wA}$  ( $S_w$ -Archie), is found using the Archie saturation formula (or Chart Sw-1) with the  $R_t$  value and known values of  $F_R$  and  $R_w$ .

An alternate  $S_w$  value, designated as  $S_{wR}$  ( $S_w$ -Ratio), is found using  $R_{xo}/R_t$  with  $R_{mf}/R_w$  as in Chart Sw-2.

If  $S_{wA}$  and  $S_{wR}$  are equal, the assumption of a step-contact invasion profile is indicated to be correct, and all values found ( $S_w$ ,  $R_t$ ,  $R_{xo}$ ,  $d_i$ ) are considered good.

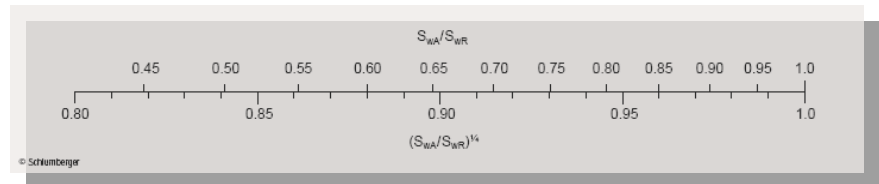
If  $S_{wA} > S_{wR}$ , either invasion is very shallow or a transition type of invasion profile is indicated, and  $S_{wA}$  is considered a good value for  $S_w$ .

If  $S_{wA} < S_{wR}$ , an annulus-type invasion profile may be indicated. In this case a more accurate value of water saturation may be estimated using the relation:

$$S_{wcor} = S_{wA} \left( \frac{S_{wA}}{S_{wR}} \right)^{\frac{1}{4}}$$

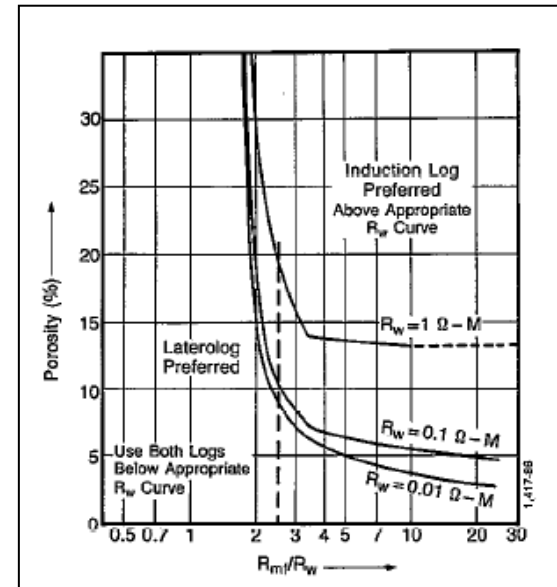
The correction factor  $(S_{wA}/S_{wR})^{1/4}$  can be found from the scale below.

For more information see Reference 9.



# Laterolog vs Induction

Both have unique characteristics that favor their use in specific, and often different, situations and application



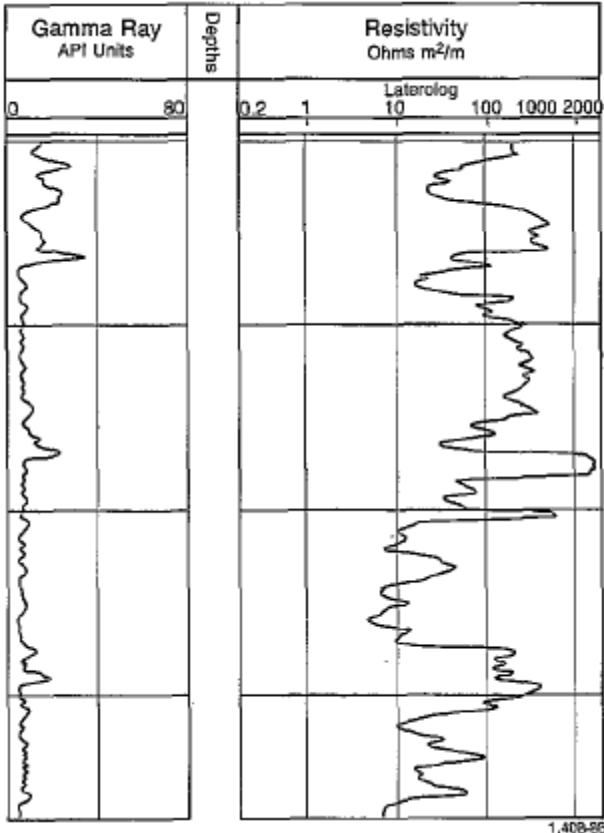
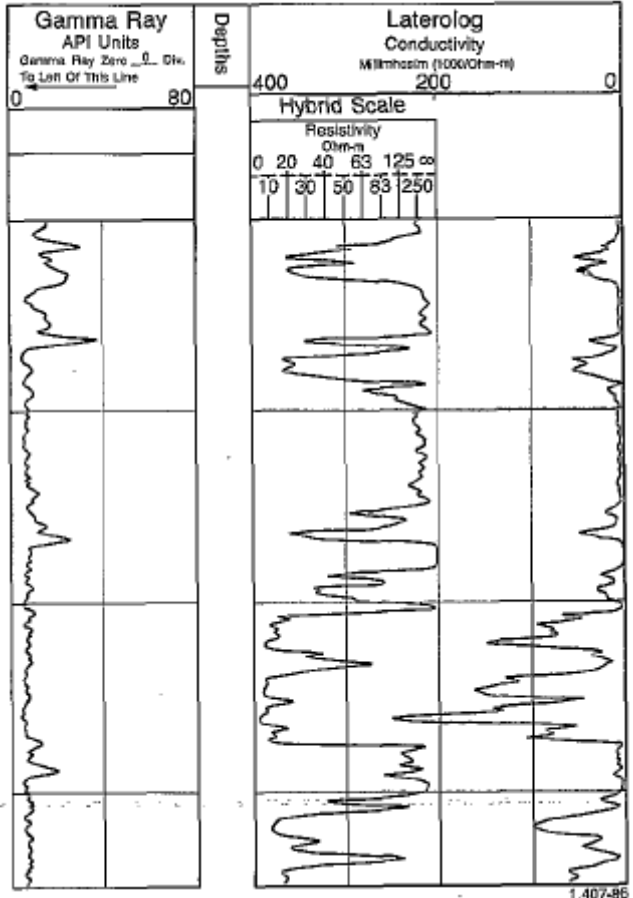
## Induction Log

- Recommended in holes drilled with moderately conductive drilling muds, non-conductive muds and in empty or air-drilled holes
- Most accurate in low- to medium-resistivity formations
- $R_{xo} > R_t$

## Laterolog

- Recommended in holes drilled with conductive muds (salt muds)
- Most accurate in medium- to high-resistivity formations
- $R_{xo} < R_t$

# Resistivity Scaling

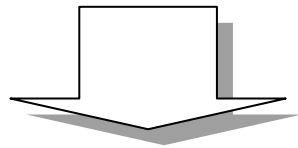


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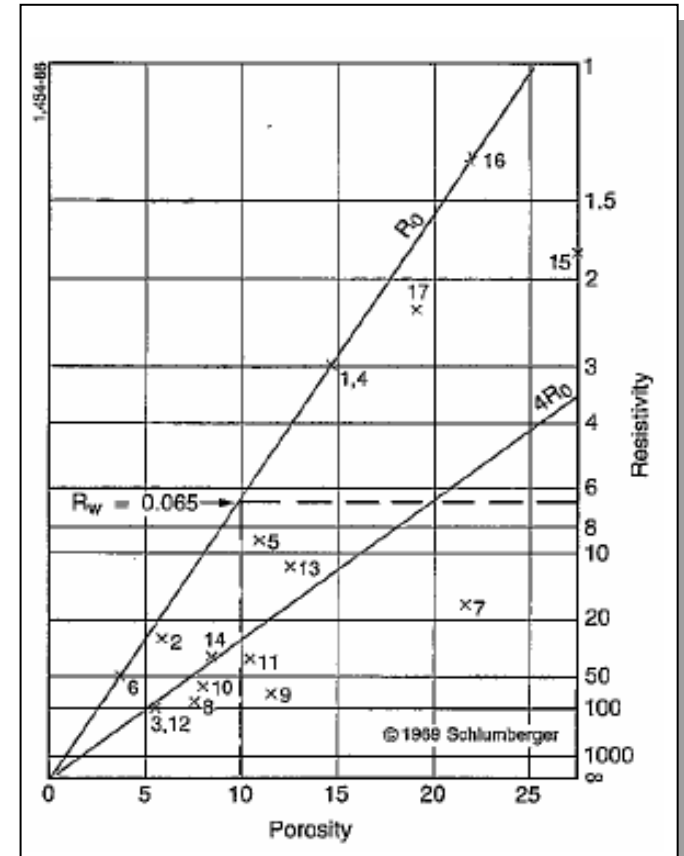
# Determination of Saturation

$$S_w = \sqrt[n]{\frac{FR_w}{R_t}} \quad F = \frac{R_0}{R_w} = \frac{a}{\phi^m}$$



$$S_w^n = \frac{aR_w}{\phi^m R_t} \quad \xrightarrow{n=m=2, a=1} \quad \phi S_w = \sqrt{\frac{R_w}{R_t}}$$

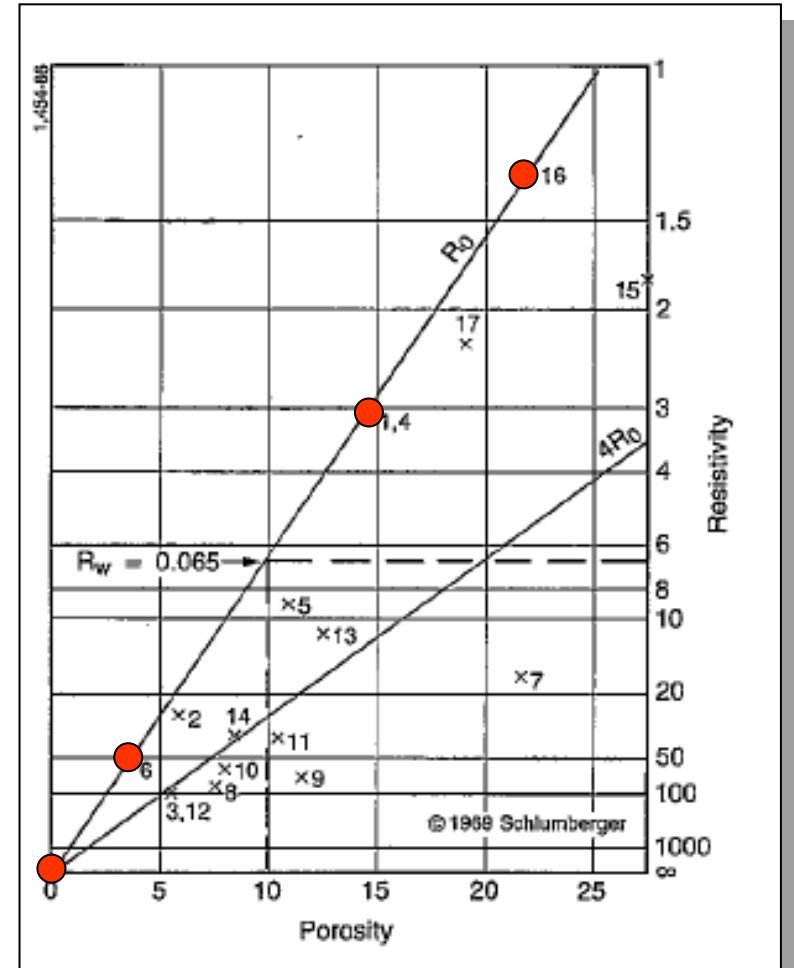
$$\rightarrow \phi = \frac{\sqrt{R_w}}{S_w} \frac{1}{\sqrt{R_t}}$$



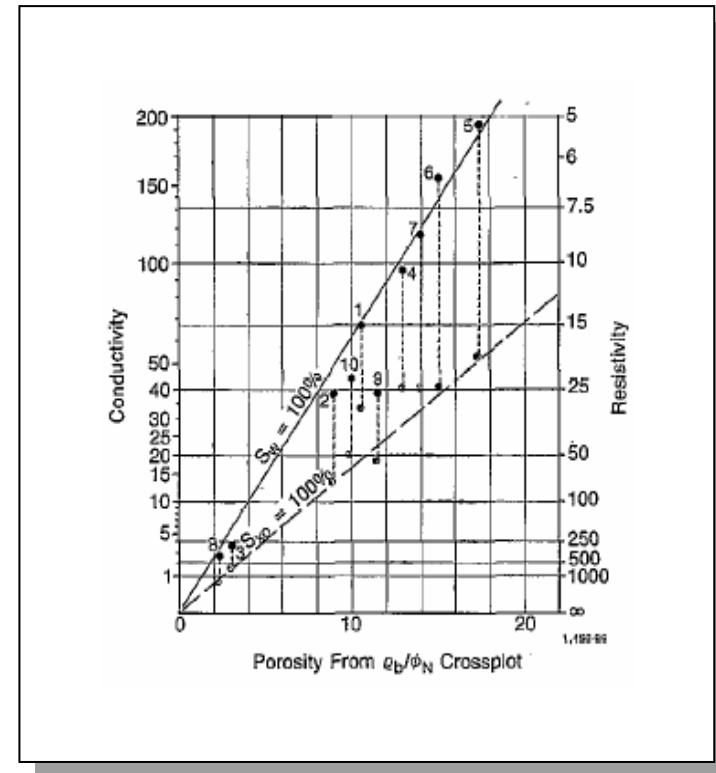
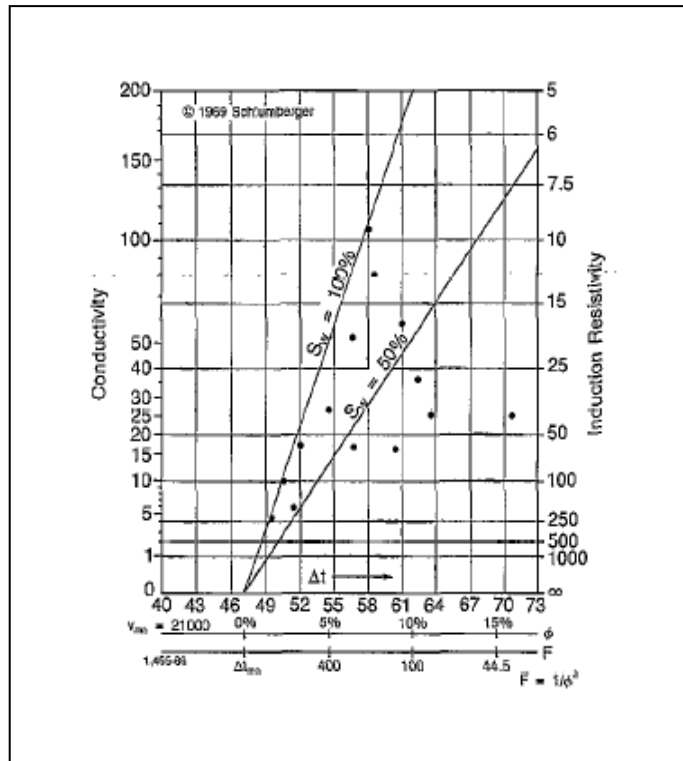
# Determination of Saturation

## EXAMPLE

- 100% water saturated formation
- $S_w = 1$ ;  $R_t = R_0$
- $R_0$  vs  $\phi$  is a straight line;  $\phi = \sqrt{R_w} / \sqrt{R_t}$
- If  $S_w \neq 1$ , but constant, all points also on a straight line
- From plotted points, assume some from 100% water saturated rock  $\rightarrow$  line through  $\phi=0$ ,  $R=\infty$  and through the most westerly plotted points
- Slope of this line defines the value of  $R_w$
- For  $\phi=10\%$ ,  $R_0 = 6.5 \text{ ohm}\cdot\text{m}$
- For compacted formations:
  - $F = 1 / \phi^2$
- So, in this case  $F = 100$
- We also now that:
  - $R_w = R_0 / F$
- So,  $R_w = 6.5 / 100 = 0.065 \text{ ohm}\cdot\text{m}$



# Determination of Saturation



- Only possible for formations with constant matrix and for constant Formation Water Resistivities