GEF4610 – OBLIGATORY EXERCISE 1 All symbols are defined in the GEF4610 Lecture Notes

Problem 1

The equations governing the Ekman currents are:

$$0 = fv + A^{(z)} \frac{d^2 u}{dz^2},$$

$$0 = -fu + A^{(z)} \frac{d^2 v}{dz^2}.$$
(1.1)

a) State the assumptions behind this set of equations.

b) We apply a constant wind stress τ along the *y*-axis at the surface z = 0, and a no-slip bottom (u = v = 0) at z = -H. Solve (1.1) and show that the complex solution W = u + iv may be written

$$W(z) = \frac{i\tau}{\rho_r a A^{(z)}} \frac{\sinh((z+H)a)}{\cosh(Ha)},$$
(1.2)

where $a^2 = if / A^{(z)}$.

c) We now consider the angle α between the wind direction and the surface velocity. Express (1.2) in terms of the Ekman depth $D_E = \pi (2A^{(z)} / f)^{1/2}$, and apply a numerical software, e.g. matlab, to plot α for various values of the ratio D_E / H . Discuss your findings.

Problem 2

a) State the assumptions leading to the equations

$$u_{t} + uu_{x} + vu_{y} - fv = -g\eta_{x} - P_{sx} / \rho,$$

$$v_{t} + uv_{x} + vv_{y} + fu = -g\eta_{y} - P_{sy} / \rho,$$

$$\eta_{t} + ((H + \eta)u)_{x} + ((H + \eta)v)_{y} = 0,$$

(2.1)

and derive the conservation equation for the potential vorticity:

$$\frac{DQ}{dt} \equiv \frac{D}{dt} \frac{f+\zeta}{H+\eta} = 0.$$
(2.2)

This means that Q is constant for a given fluid column. We will use these equations on an f-plane, and consider steady flow in this problem.

b) We have constant geostrophic flow U_0 in the x-direction in a layer of constant depth H_0 . What are the surface pressure gradients in this case? c) We introduce a small sub-sea ridge q(x) of width 2*L* which is infinitely long in the *y*-direction. The fluid depth then becomes $H = H_0 - q$; see Fig. 1.

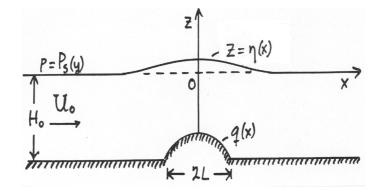


Figure 1. Figure sketch.

The flow will now be modified. The velocities in the x- and y-directions can be written $U_0 + u(x)$ and v(x), respectively, where u and v are small compared to U_0 . Assume that the velocity far upstream of the ridge is U_0 , the depth is H_0 , and the relative vorticity is zero. Show from (2.2) that

$$v_x = \frac{f}{H_0} (\eta - q).$$
 (2.3)

d) Show that the linearized momentum equations in (2.1) becomes

$$U_{0}u_{x} - fv = -g\eta_{x},$$

$$U_{0}v_{x} + fu = 0.$$
(2.4)

e) Combine (2.3) and (2.4), and show that

$$(1 - F_0^2)\eta_{xx} - \frac{1}{a^2}\eta = -F_0^2 q_{xx} - \frac{1}{a^2}q, \qquad (2.5)$$

where

$$F_0 = \frac{U_0}{(gH_0)^{1/2}}, \quad a = \frac{(gH_0)^{1/2}}{f}.$$
 (2.6)

 F_0 and a are important fluid parameters. What is their significance?

f) Assume subcritical flow, and take that $\eta \to 0, x \to \pm \infty$. Use that d/dx^2 scales as $1/L^2$ in order to simplify (2.5). Discuss the surface elevation over the ridge in the extreme cases $L^2 \ll a^2$, and $L^2 \gg a^2$.

g) Sometimes the rigid lid approximation is used for flow over a ridge (the surface is horizontal everywhere). Now (2.3) reduces to

$$v_x = -\frac{f}{H_0}q, \qquad (2.7)$$

i.e. anti-cyclonic relative vorticity is generated over the entire ridge. Show from (2.7) that v downstream of the ridge is constant, and dependent on the cross-sectional area A of the ridge, given by

$$A = \int_{-L}^{L} q(x) dx.$$
 (2.8)

h) Use the continuity equation in (2.1), and find *u* in this case.

i) Show that the angle between the current upstream of the ridge and the current downstream of the ridge in the case of a rigid lid is given by

$$\theta = \arctan\left(\frac{fA}{U_0H_0}\right). \tag{2.9}$$