

INF5410 Array signal processing. Chapter 2.4 Refraction and diffraction

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Deviations from simple media

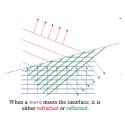
- 1. Dispersion: $c = c(\omega)$
 - Group and phase velocity, dispersion equation: $\omega = f(k) \neq c \cdot k$
 - Evanescent (= non-propagating) waves: purely imaginary k
- 2. Attenuation: $c = c_{\Re} + jc_{\Im}$
 - Wavenumber is no longer real, imaginary part gives attenuation.
 - Waveform changes with distance
- 3. Non-linearity: c = c(s(t))
 - Generation of harmonics, shock waves
- 4. Refraction: c=c(x,y,z)
 - Snell's law

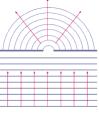
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Reflection, refraction, diffraction

 Click http://lectureonline.cl.msu.edu/~mmp/kap13/cd372.htm





A wave is diffracted by an aperture.

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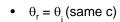


4. Refraction - avbøyning

· Unchanged phase on interface:

$$\overrightarrow{k_i} \cdot \overrightarrow{x} = \overrightarrow{k_r} \cdot \overrightarrow{x} = \overrightarrow{k_t} \cdot \overrightarrow{x}$$
 • Fig 2.10:

$$|\overrightarrow{k_i}| \cdot \sin \theta_i = |\overrightarrow{k_r}| \cdot \sin \theta_r = |\overrightarrow{k_t}| \cdot \sin \theta_t$$



- Snell's law: $sin\theta_i/c_i = sin\theta_t/c_t$
- Willebrand Snell von Royen, NL 1591-1626







Critical Angle - total reflection

- Total reflection for all θ_{ι} which result in $\theta_{t}{>}90^{0}$
- Critical angle sinθ_i=c_i/c_t
- Ex: steel c_t =5800 m/s, water c_i =1490 m/s, θ_i <16.50
- Important for containing 100% of transmitted energy inside optical fibers

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5



Simple model for the sea

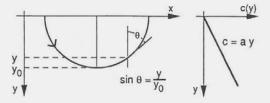


Figure 2.11 A linear change in the speed of sound with depth results in circular rays. The linear sound profile is shown in the right panel.

Problem 2.8. More general: $c=c_0(1+ay)$

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Linear speed variation, c(y)=ay

- Find $\theta(y)$ when wave is horizontal at depth y_0
- Snell's law: $\frac{\sin \theta(y)}{c(y)} = \frac{\sin \theta(y \delta y)}{c(y \delta y)}$
- Multiply by $c(y-\delta y)$ and subtract $sin\theta(y)$

$$\sin\theta(y-\delta y) - \sin\theta(y) = \frac{\sin\theta(y)}{c(y)} \cdot [c(y-\delta y) - c(y)]$$

• In the limit:

$$\frac{1}{\sin\theta(y)}\frac{d\sin\theta}{dy} = \frac{1}{c(y)}\frac{dc}{dy}$$

y y_0 y $\sin \theta = \frac{y}{y_0}$

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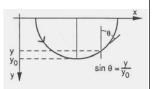


- Equation: $\frac{1}{\sin \theta(y)} \frac{d \sin \theta}{dy} = \frac{1}{c(y)} \frac{dc}{dy}$
- Solution: $\ln(\sin\theta) = \ln(c) + C_0$ $\sin\theta(y) = C_1 c(y)$
 - Linear variation: c(y)=ay
 - Boundary condition: $\sin\theta(y_0)=1 \Rightarrow C_1=1/ay_0$
- · Final solution:

$$\sin\theta = C_1 c(y) = ay/ay_0 = y/y_0$$

A circle with radius y₀

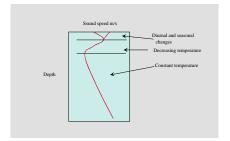






Underwater acoustics: Sound speed profiles

 $c = 1448.6 + 4.618T - 0.0523T^2 + 1.25(S - 35) + 0.017D$.



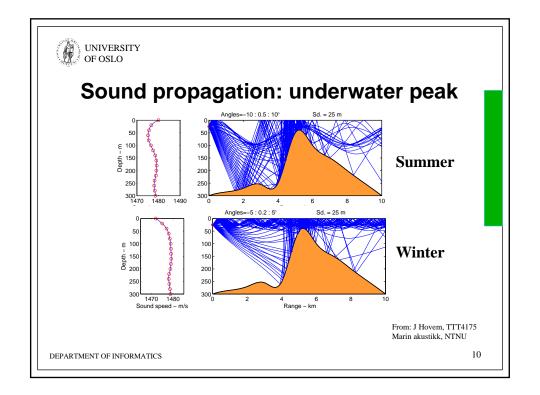
Empirical law:

- •c = velocity of sound (m/s),
- •T = temperature (°C),
- •S = salinity (per thousand, promille),
- •D = depth (m).

Fra: J Hovem, TTT4175 Marin akustikk, NTNU

9

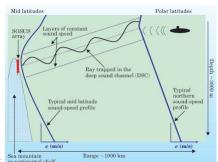
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Deep sound channel

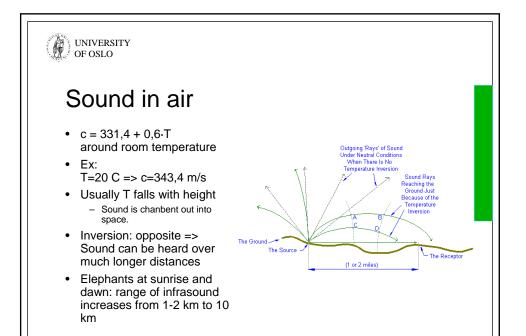
- c decreases as the water cools but increases with depth.
- Deep sound channel (DSC)
- From the cold surface at the poles to ~1300 m at the equator
- Sound can propagate thousands of kilometers
- 1950s: US Navy SOSUS (Sound Ocean Surveillance System) network to monitor Soviet submarines.
- Kuperman and Lynch, "Shallowwater acoustics", Physics Today, 2004

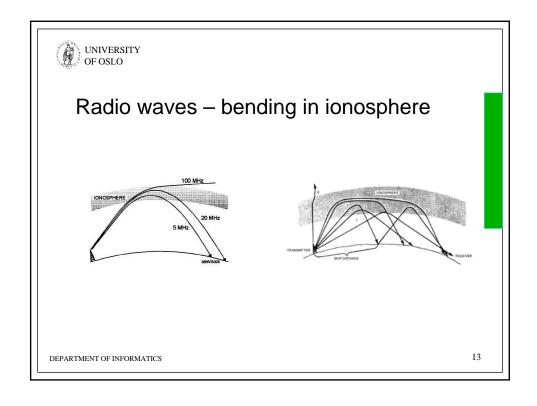


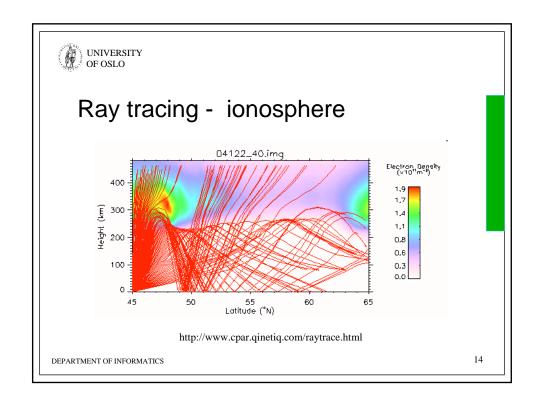
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11





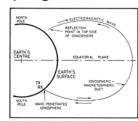




Ionosphere - odd propagation

Echo of 0.15-0.3 sec for frequencies 1-4 MHz, i.e. Up to 2-45.000 km \approx 2.7 earth radii

- G. T. Goldstone and G. R. A. Ellis, "Observations of 1.91 MHz echoes from the magnetic conjugate point after propagation through a magneto-ionic duct," Proc. Astronom. Soc Australia (3), 1986, pp 333-335
- S. Holm, Radiosignaler med mange sekunders forsinkelse, Fra Fysikkens Verden, side 110-113, nr 4, 2004





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2.4.2 Ray Theory

- Method for finding ray path based on geometry alone = high frequency approximation
- Read the details in the book if you need to understand better underwater acoustics or modeling of the ionosphere!

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Periodic media

250-mm-long steel cylinder rods lattice constant $a=2.5 \, mm$ radius of cylinders: R=1.0 mm Csteel = 6100 m/s, cair = 334.5 m/sf = 41.2 to 48.0 kHz

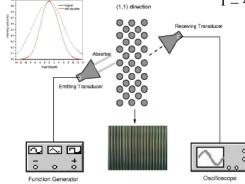


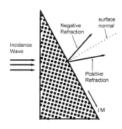
FIG. 2. (Color online) Sche-matic of the experimental setup-used to measure the transmission of ultrasonic wave in a SC, consisting of two transducers, a flat rectangular slab of steel cylinders, rectangular slab of steel cylinders, a function generator, and an oscil-loscope. The SC, the rectangular slab of steel cylinders shown as the middle-bottom inset, is placed between two transducers and the left-top inset shows measurements of the amplitude comparisons with the absorber (solid) to without the absorber (solid) to without the absorber (solid) to

Feng, Liu, Chen, Huang, Mao, Chen, Li, Zhu, Negative refraction of acoustic waves in two-dimensional sonic crystals, Physical Review B, 2005

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Periodic media



Zhanga, Liu: Negative refraction of acoustic waves in two-dimensional phononic crystals, Applied Physics Letters, 2004.

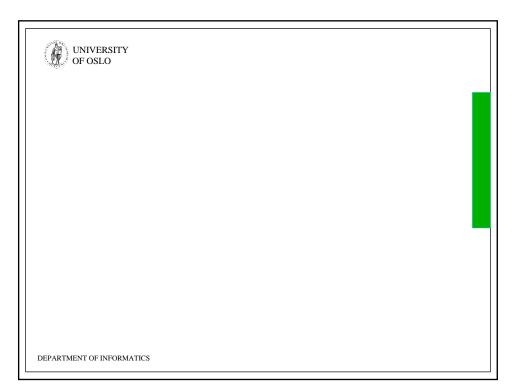
- Acoustic metamaterials can manipulate sound waves in surprising ways, which include collimation, focusing, cloaking, sonic screening and extraordinary transmission.
- Recent theories suggested that imaging below the diffraction limit using passive elements can be realized by acoustic superlenses or magnifying hyperlenses. These could markedly enhance the capabilities in underwater sonar sensing, medical ultrasound imaging and nondestructive materials testing.
- Li et al, Experimental demonstration of an acoustic magnifying hyperlens, 18 Nature 2009



Array Processing Implications

- Spatial inhomogeneities must be taken into account by array processing algorithms
 - The essence of matched field processing
- Waves propagating in an inhomogenous medium rarely travel in a straight line
 - Makes array processing/beamforming much harder
- Refraction can lead to multipath
 - Can be modeled as a low-pass filter, e.g. loss of high frequencies

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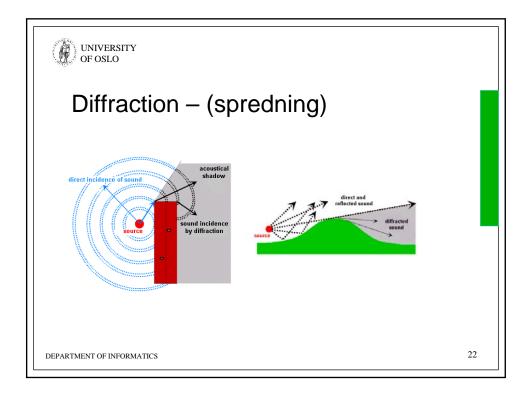




Diffraction

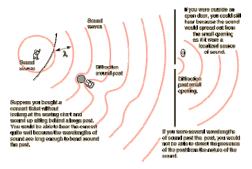
- Ray theory: Geometrical model of optics
- High-frequency small wavelength model
- Diffraction:
 - Wavelength comparable to structure size
 - Edges of shadows are not perfectly sharp
 - Can hear around corners
- In this course: mainly consequences of diffraction

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Diffraction



• Geometric acoustic is OK for dimensions > 1 wavelength

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23



Huygens' principle

- Christian Huygens, NL, 1629-1695
- Each point on a travelling wavefront can be considered as a secondary source of spherical radiation
- Also a model for an oscillating piston = acoustic source



Figure 2.13 A wave is shown impinging on a hole in a planar screen. The Rayleigh-Sommerfel diffraction formula tells us what the wavefield at the point \vec{x} is in terms of the wavefield at the aperture.

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Mathematical formulation of diffraction

- Augustin Jean Fresnel (F) 1788 1827
- Gustav Robert Kirchhoff (D) 1824 1887
- Lord Rayleigh, John William Strutt (GB) 1842
 1919, Nobel prize physics, 1904.
- Arnold Johannes Wilhelm Sommerfeld (D) 1868 – 1951
- Joseph von Fraunhofer (D) 1787 1826

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25



Diffraction: deviation from geometrical model

• Rayleigh-Sommerfeld diffraction formula from a hole with aperture A:

$$s(\overrightarrow{x}) = \frac{1}{j\lambda} \int \int_A s(\overrightarrow{x}_h) \frac{\exp\{jkr\}}{r} \cos\theta dA$$

- Wave at x is a superposition of fields from the hole, due to linearity of wave equation
- Weighted by a spherical spreading function exp{jkr}/r
- Also weighted by $1/\lambda$
- Obliquity factor cosθ
- Phase shift of $\pi/2$ due to 1/j



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Two approximations

- Fresnel, nearfield, (but not quite near)
- · Fraunhofer, farfield
- Leads to
 - important estimates for nearfield farfield transition distance
 - Fourier relationship between aperture excitation and field

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27



Fresnel approximation

$$s(\overrightarrow{x}) = \frac{1}{j\lambda} \int \int_A s(\overrightarrow{x}_h) \frac{\exp\{jkr\}}{r} \cos\theta dA$$

- $\cos \theta \approx 1$, $r \approx d$ for amplitude
- Phase:
 - spherical surfaces \approx quadratic
 - parabolic approximation

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Fresnel derivation

- Point in the hole $(\tilde{x}, \tilde{y}, 0)$, in observation plane (x,y,z=d)
- Distance: $r = [(x \tilde{x})^2 + (y \tilde{y})^2 + d^2]^{1/2}$ $r = d[1 + \frac{(x \tilde{x})^2 + (y \tilde{y})^2}{d^2}]^{1/2}$
- Approximate (1+x)¹/2≈1+x/2, i.e. small x/D ⇔ small angles

$$r \approx d + \frac{(x - \tilde{x})^2 + (y - \tilde{y})^2}{2d}$$

• Use the above expression for the phase and r≈d for the amplitude in Rayleigh-Sommerfeld integral

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29



Fresnel approximation

$$s(x,y) = \frac{exp\{jkd\}}{j\lambda d} \int \int_A s(\tilde{x},\tilde{y}) \exp\left\{\frac{jk[(x-\tilde{x})^2 + (y-\tilde{y})^2]}{2d}\right\} d\tilde{x}d\tilde{y}$$

- Nearfield approximation & within $\approx 15^{\circ}$ of z-axis
- · Also called paraxial approximation
- 2D convolution between field in hole and h(x,y):

$$h(x,y) = \frac{exp\{jkd\}}{j\lambda d} \exp\left\{\frac{jk(x^2 + y^2)}{2d}\right\}$$

 This is a quadratic phase function = the phase shift that a secondary wave encounters during propagation

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Fraunhofer approximation

• Expand phase term in Fresnel approximation

$$s(x,y) = \frac{\exp\{jkd\}}{j\lambda d} \int_A s(\tilde{x},\tilde{y}) \exp\{\frac{jk[(x-\tilde{x})^2 + (y-\tilde{y})^2]}{2d}\} d\tilde{x} d\tilde{y}$$

and neglect quadratic phase term variation over hole

$$(x-\tilde{x})^2 + (y-\tilde{y})^2 = x^2 + y^2 - 2x\tilde{x} - 2y\tilde{y} + (\tilde{x}^2 + \tilde{y}^2) \approx x^2 + y^2 - 2x\tilde{x} - 2y\tilde{y}$$

• If D = max linear dimension of hole, this is equivalent to assuming (d=dist. from source):

$$\frac{\tilde{x}^2}{2d} \le \frac{(D/2)^2}{2d} << \lambda/2 \Longrightarrow d >> \frac{D^2}{4\lambda} \leftarrow$$
Fresnel limit

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31



Fraunhofer approximation

$$s(x,y) = \frac{exp\{jkd\}}{j\lambda d} \exp{\{\frac{jk(x^2+y^2)}{2d}\}} \int\!\int_A s(\tilde{x},\tilde{y}) \exp{\{\frac{jk(x\tilde{x}+y\tilde{y})}{d}\}} d\tilde{x} d\tilde{y}$$

- Far-field approximation: valid far away from hole
- s(x,y) = 2D Fourier transform of field in hole

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Fourier transform relationship

- Very important result
- Link between the physics and the signal processing!
- Basis for simplified expressions like angular resolution $\approx \lambda/D$ etc
- Small hole leads to wide beam and vice versa just like a short time-function has a wide spectrum

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33

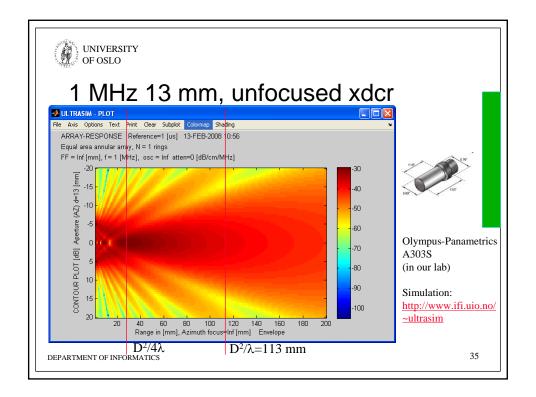


Nearfield-farfield limit

Not a clear transition, several limits are used, in increasing size:

- $d_F = D^2/4\lambda$: Fresnel limit
- $d = \pi r^2/\lambda = \pi/4 \cdot D^2/\lambda$: Diffraction limit
- d = D^2/λ : max path length difference $\lambda/8$
- $d_R = 2D^2/\lambda$: Rayleigh dist: Δ path = $\lambda/16$
- Proportional to D²/λ, multiplied by 0.25, 0.79, 1, or 2

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Array Processing Implications

- Diffraction means that opaque objects located between the source and the array can induce complicated wavefields
 - Scattering theory:
 - » Acoustics: Schools of fish
 - » Electromagnetics: rain drops
 - » Complicated, but important to understand

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Norsk terminologi

- Bølgeligningen
- Planbølger, sfæriske bølger
- Propagerende bølger, bølgetall
- Sinking/sakking: $\overrightarrow{\alpha}$
- Dispersjon
- Attenuasjon eller demping
- Refraksjon
- Ikke-linearitet
- Diffraksjon; nærfelt, fjernfelt
- Gruppeantenne (= array)

Kilde: Bl.a. J. M. Hovem: ``Marin akustikk", NTNU, 1999