INF 5490 RF MEMS

L12: Micromechanical filters

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Today’s lecture

- Properties of mechanical filters
- Visualization and working principle
- Design, modeling
- Examples
  - 2 resonator c-c beam structure for HF-VHF
  - comb structure
- Design procedure
- Mixer

Mechanical filters

- Well-known for several decades
  - Jmfr. book: ”Mechanical filters in electronics”, R.A. Johnson, **1983**
- **Miniaturization** of mechanical filters makes it more interesting to use
  - Possible by using micromachining
  - Motivation → Fabrication of small integrated filters: ”system-on-chip” with good filter performance

Filter response

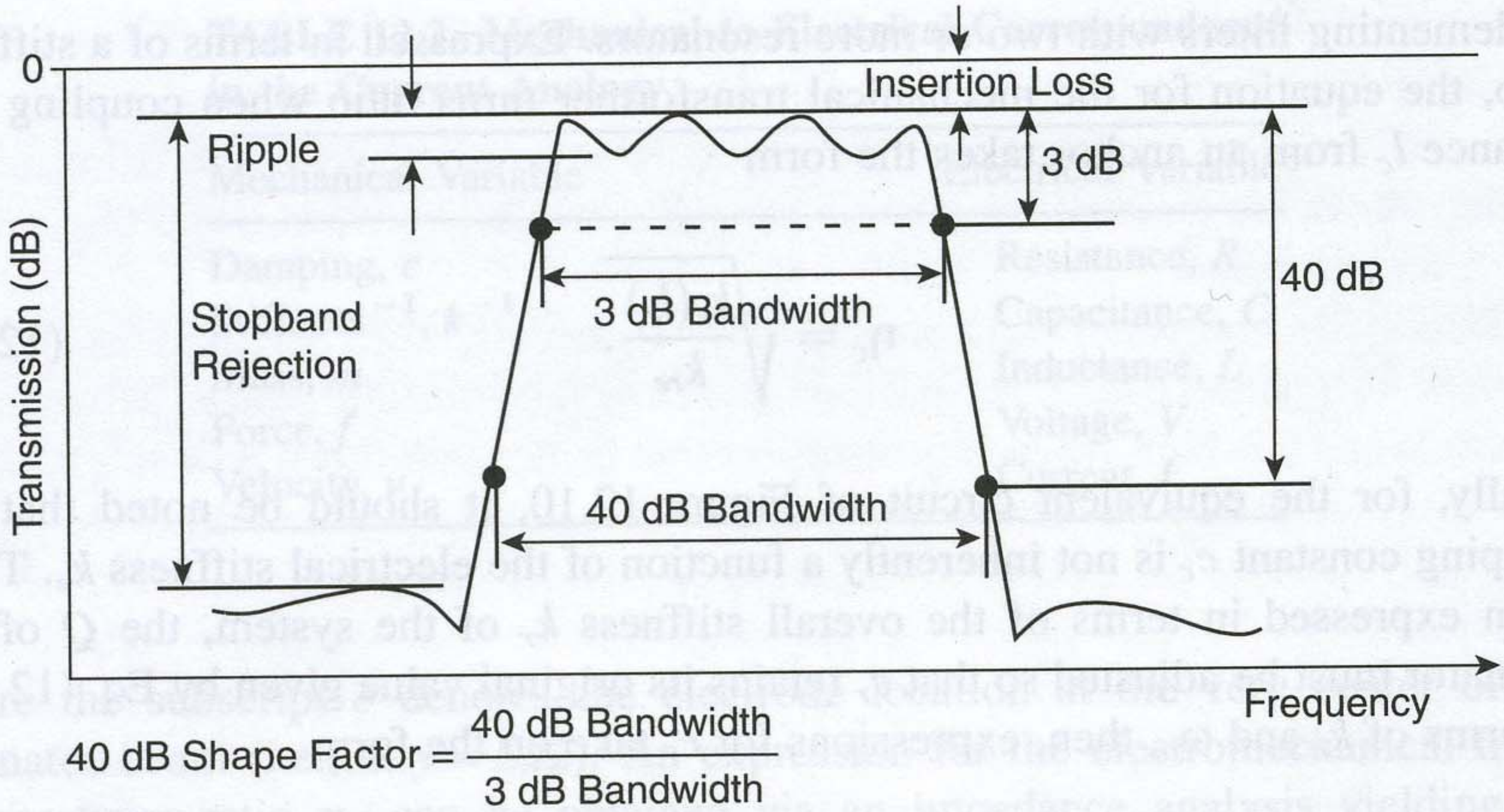


Figure 12.11. Parameters typically used for filter specification. (From reference [29])

Several resonators used

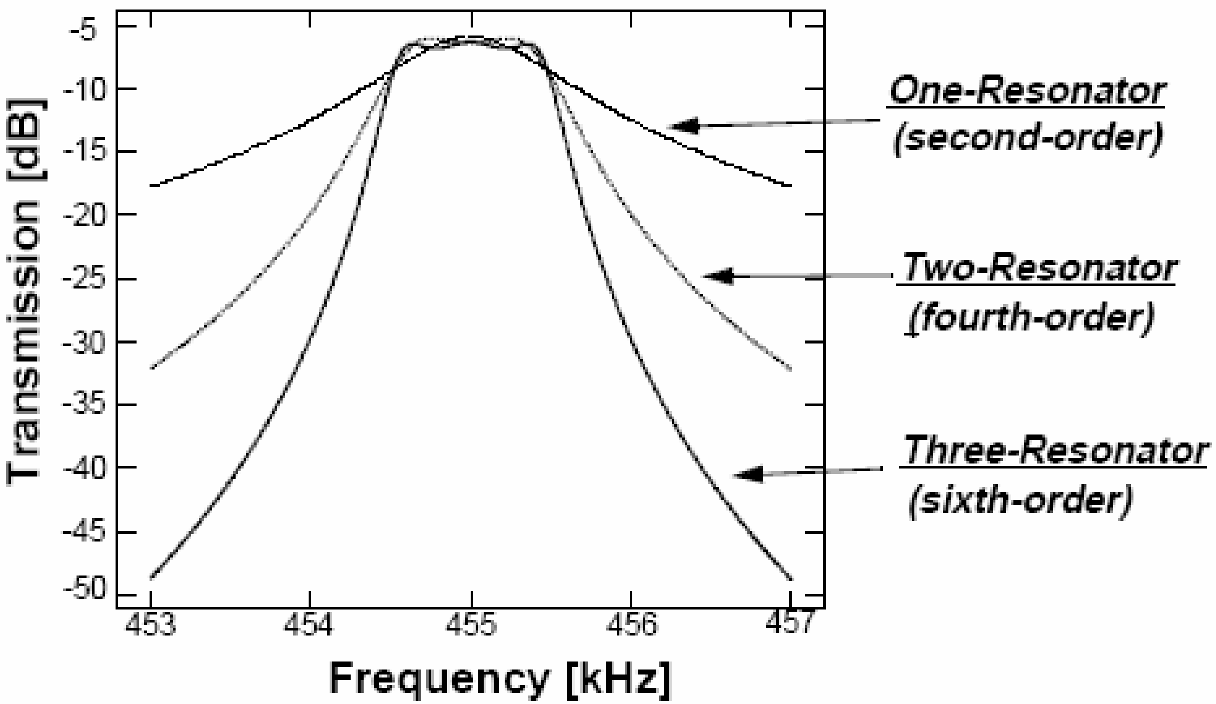
- One **single** resonator has a narrow BP-response
  - Good for defining oscillator frequency
  - Not good for BP-filter
- BP-filters are implemented by coupling resonators in cascade
  - Gives a wider pass band than using one single resonating structure
  - 2 or more micro resonators are used
    - Each of comb type or c-c beam type (or other types)
  - **Connected by soft springs**

Filter order

- Number of resonators, n, defines the filter **order**
  - Order = 2 * n
  - Sharper ”roll-off” to stop band when several resonators are used
    - → ”sharper filter”

Attaining Better Performance

- Use more resonators to attain higher order
- Filter Order = 2 x (# of resonators)

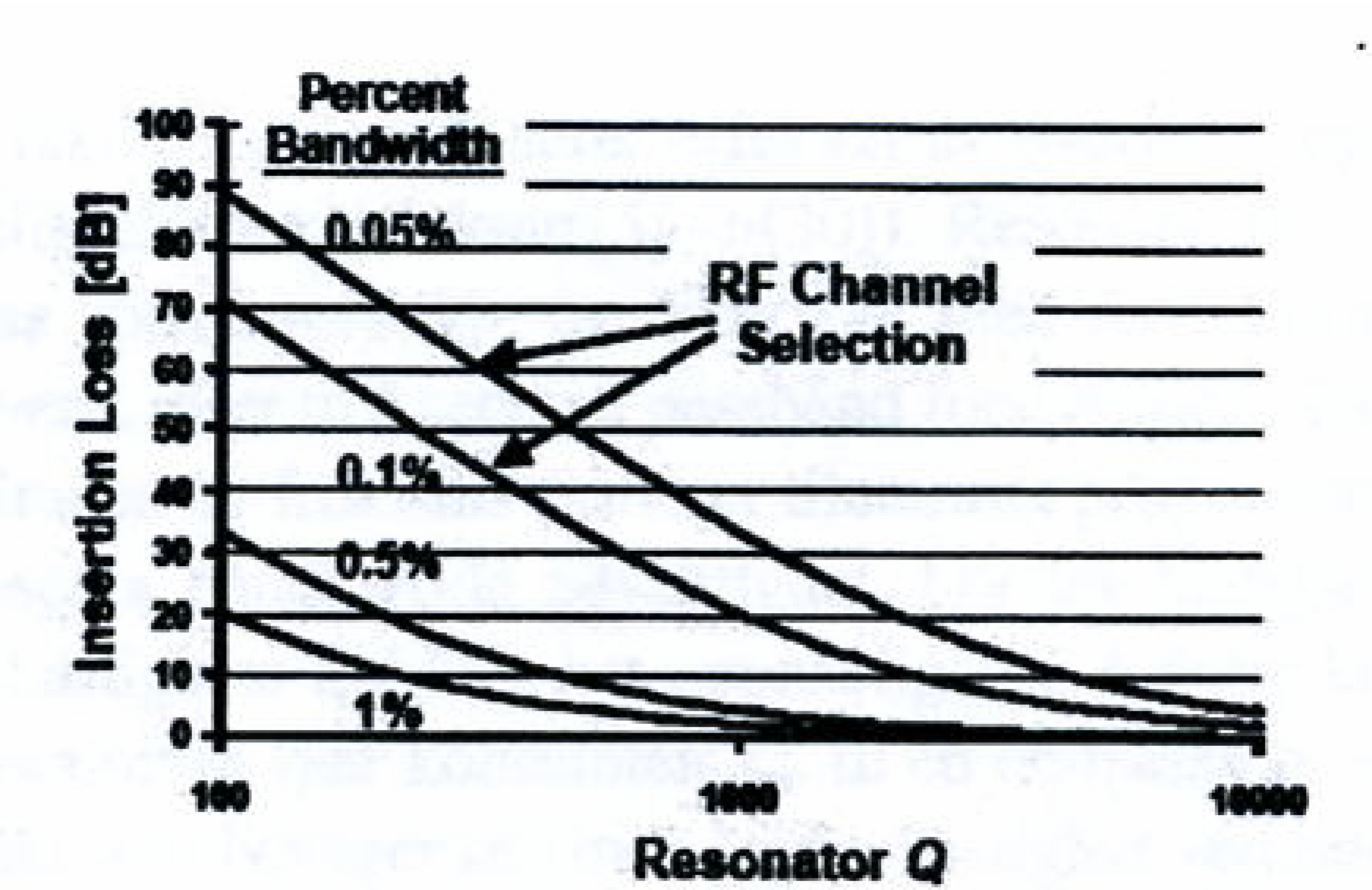


- Higher order ➠ sharper roll-off ➠ better stopband rejection

Micromachined filter properties

- **Compact** implementation
  - ”on-chip” filter bank possible
- **High Q-factor** can be obtained
- **Low-loss BP-filters** can be implemented
  - The individual resonators have low loss
  - Low total ”Insertion loss”
    - IL: Degraded for small bandwidth →
    - IL: Improved for high Q-factor →

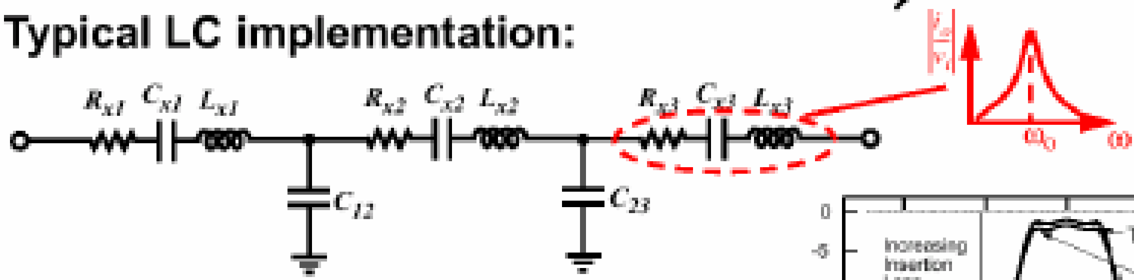
”Insertion loss”



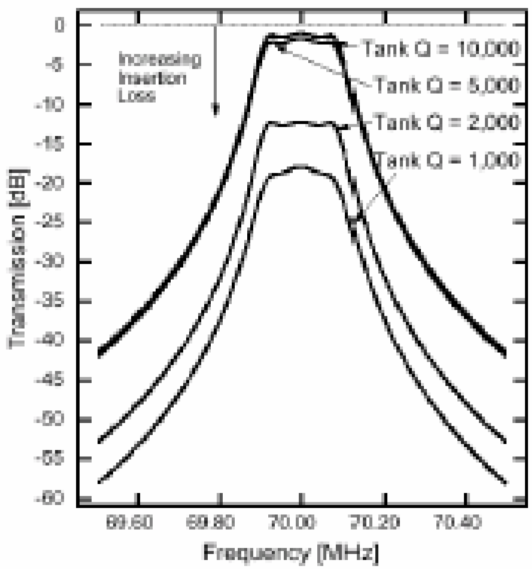
Importance of High Q: Low Loss Filters

General BPF Implementation

Typical LC implementation:



- In resonator-based filters: high tank *Q* ⇔ low insertion loss
- <u>At right</u>: a 0.3% bandwidth filter @ 70 MHz (simulated) — heavy insertion loss for resonator *Q* < 5,000



Illustrating principle: 3 * resonators

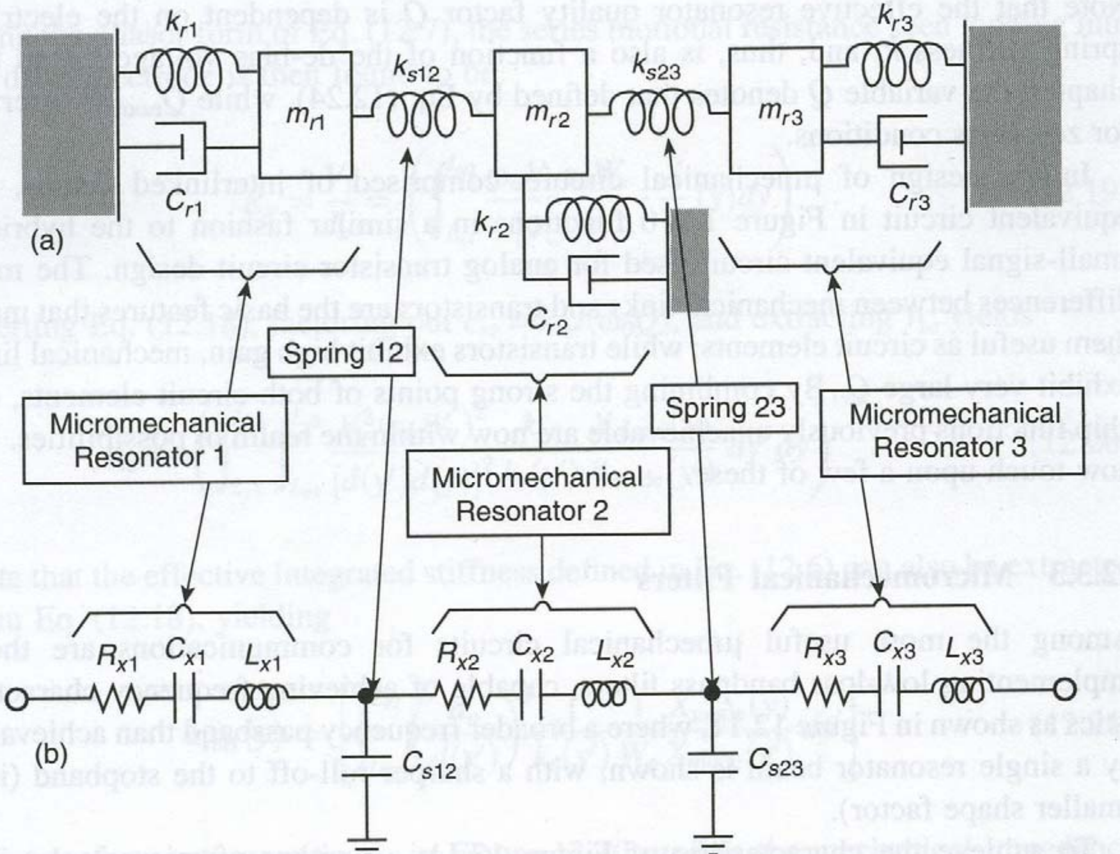
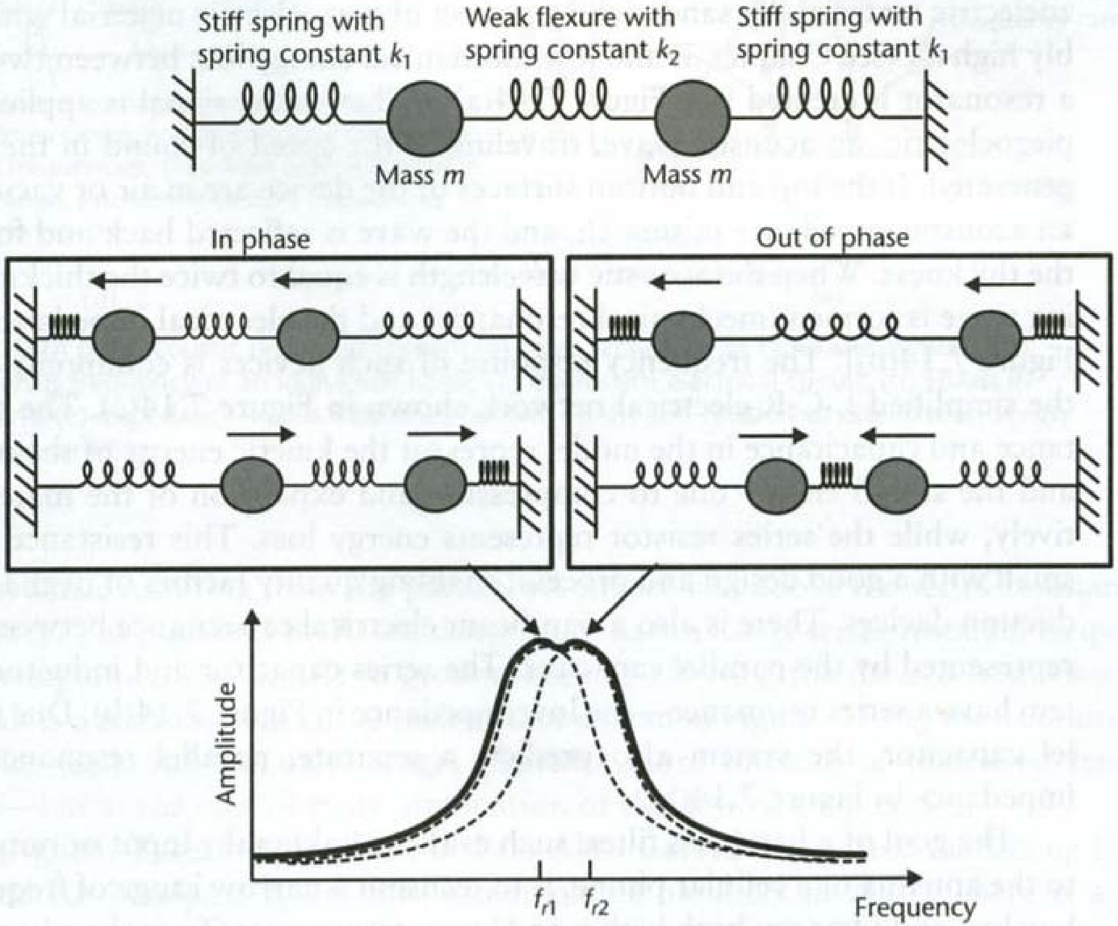


Figure 12.12. (a) Equivalent lumped-parameter mechanical circuit for a mechanical filter. (b) Corresponding equivalent *LCR* network.

Mechanical model

- A coupled resonator system has several **vibration modes**
- n independent resonators
  - Resonates at their natural frequencies determined by m, k
  - **”compliant”** coupling spring
    - Determines the resulting **resonance modes** of the many-body system

Visualization of the working principle



$$f_{r1} = \frac{1}{2\pi}\sqrt{\frac{k_1}{m}} \quad f_{r2} = \frac{1}{2\pi}\sqrt{\frac{k_1 + 2\,k_2}{m}}$$

Figure 7.13 Illustration of two identical resonators, each with a mass and spring, coupled by a weak and compliant intermediate flexure. The system has two resonant oscillation modes, for in-phase and out-of-phase motion, resulting in a bandpass characteristic.

Visualization of the working principle, contd.

- 2 oscillation modes in figure 7.13
  - In phase
    - No relative displacement between masses
    - No force from coupling spring
    - Oscillation frequency = natural frequency for a single resonator (both are equal, - **"mass less"** coupling spring*****)
      - (***** actual coupling spring mass can lower the frequency)
  - Out of phase
    - Displacement in opposite directions
    - Force from coupling spring (added force)
    - Gives a higher oscillation frequency (Newton's 2.law, F=ma)
    - → the 2 overlapping resonance frequencies are **split** into 2 distinct frequencies

3-resonator structure

- Each vibration mode corresponds to a **distinct top** in the frequency response
  - Lowest frequency: all in phase
  - Middle frequency: center not moving, ends out of phase
  - Highest frequency: each 180 degrees out of phase with neighbour

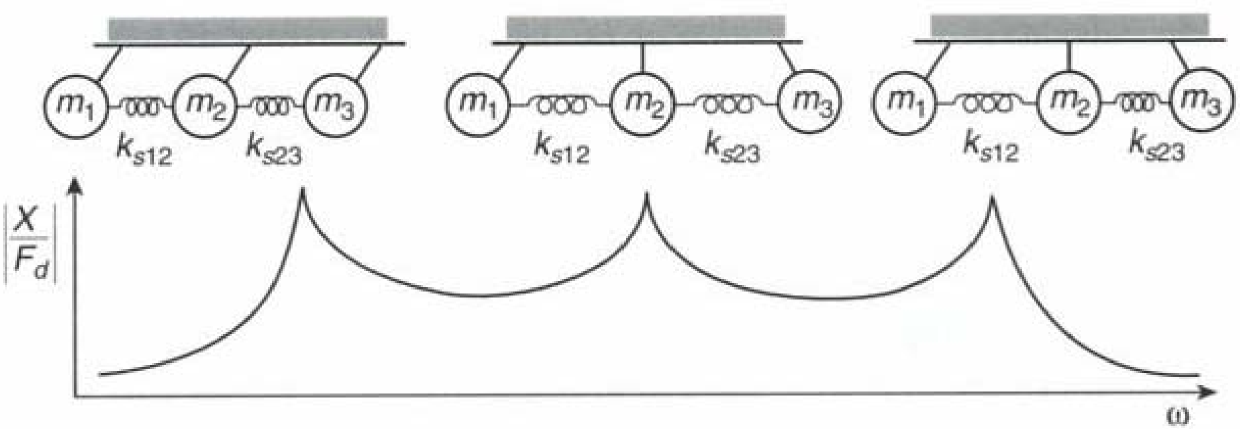
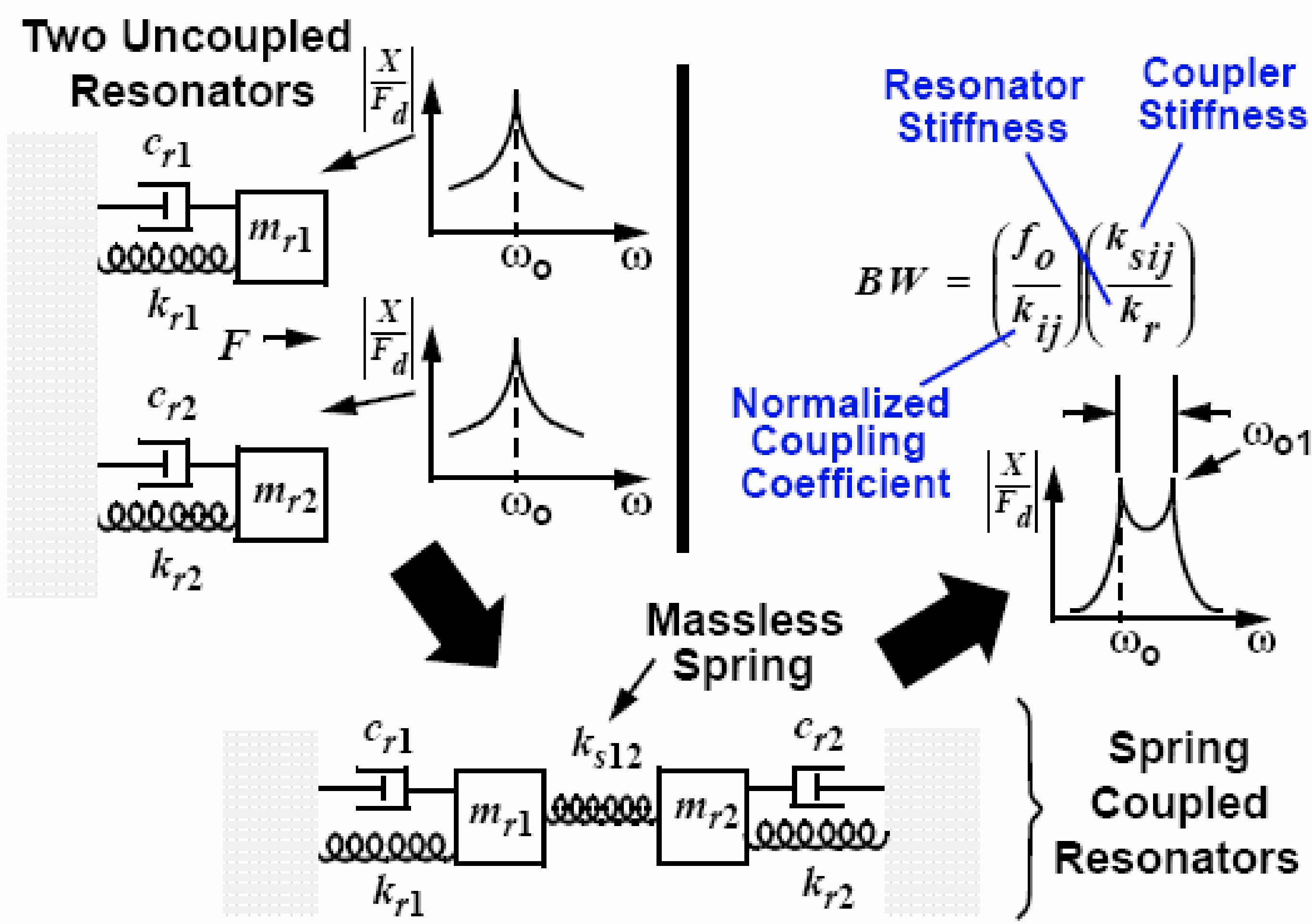


Figure 12.13. Mode shapes of a three-resonator micromechanical filter and their corresponding frequency peaks.

Filter response

- **Frequency separation** depends on the stiffness of the coupling spring
  - Soft spring (”compliant”) → close frequencies = narrow pass band
- Increased number of coupled resonators in a linear chain gives
  - Wider pass band
  - **Increased number of passband ”ripples”**
  - → the total number of oscillation modes are equal to the number of coupled resonators in the chain

Ideal Spring Coupled Filter



$$BW = \left(\frac{f_o}{k_{ij}}\right)\left(\frac{k_{sij}}{k_r}\right)$$

Design

- Resonators used in micromechanical filters are normally **identical**
  - Same dimension and resonance frequency
  - Filter centre frequency is f_0
    - ("massless coupling spring")
- Pass band determined by max distance between node tops
  - Relative position of vibration tops is determined by
    - Coupling spring stiffness k_{sij}
    - Resonator properties (spring constant) k_r at coupling points

Design, contd.

- At centre frequency f_0 and bandwidth B, spring constants must fulfill

$$B = \left(\frac{f_0}{k_{ij}}\right) \cdot \left(\frac{k_{sij}}{k_r}\right)$$

  - k_{ij} = normalized coupling coefficient taken from filter cook books
  - **Ratio** $\left(\frac{k_{sij}}{k_r}\right)$ important, NOT absolute values

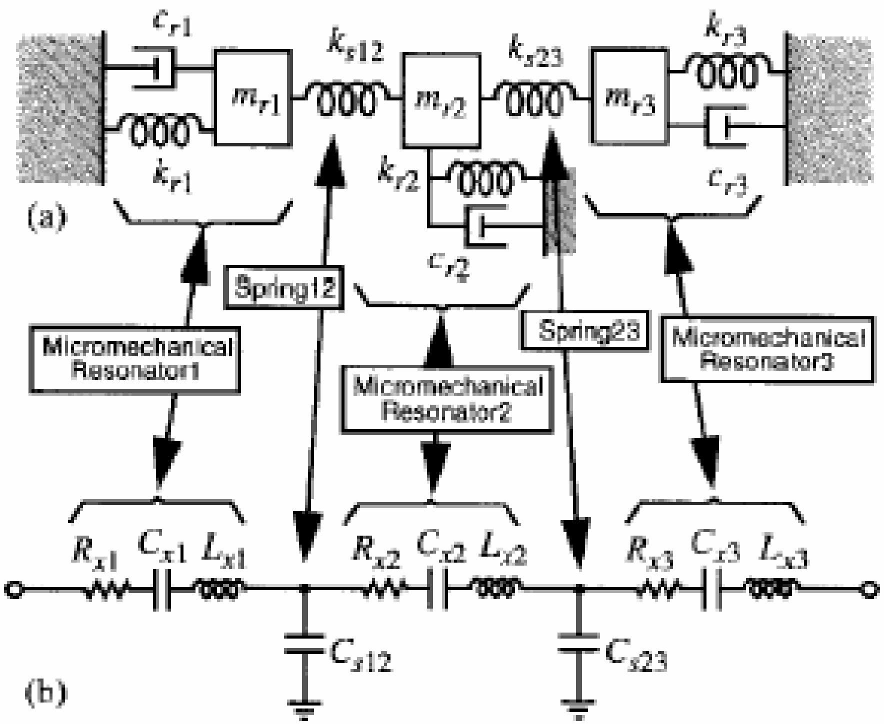
- **Theoretical** design procedure *

- (* can not be implemented)
  - Determine f_0 and k_r Choose k_{sij} for required B
  - I real life this procedure is **modified** (discussed later →)

Mechanical or electrical design?

- Much similarity between description of mechanical and electrical systems
- The **dual** circuit to a ”spring-mass-damper” system is a **LC-ladder network →**
  - Electromechanical analogy used for conversion
  - Each resonator a LCR tank
  - Each coupling spring (idealized massless) corresponds to a shunt capacitance

High-Order Micromechanical Filters: Lumped Mechanical Model and Its Equivalent LCR Circuit



Analogies

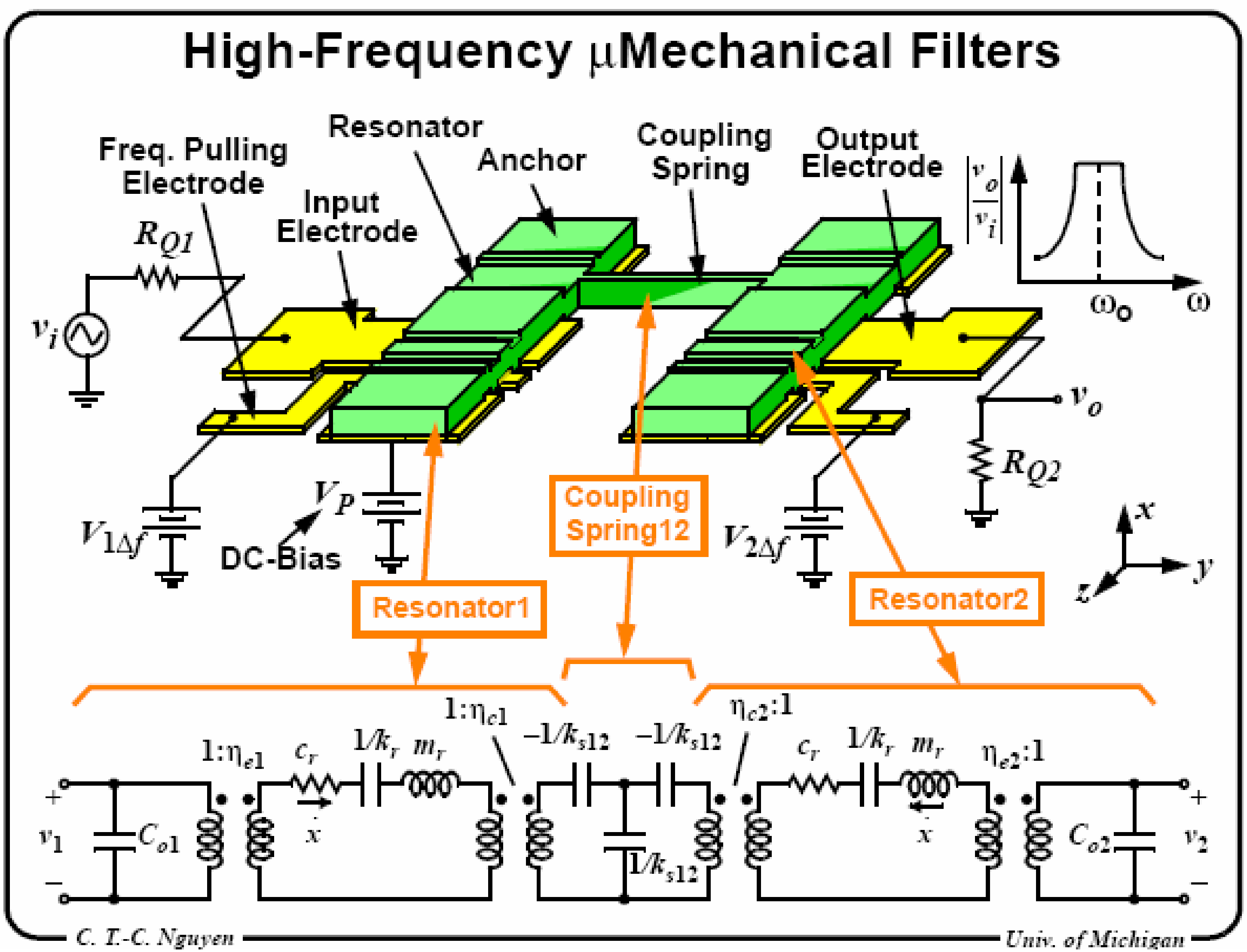
C - k

L - m

Modeling

- Systems can be modeled and designed in **electrical domain** by using procedures from coupled resonator ”ladder filters”
  - All polynomial syntheses methods from electrical filter design can be used
  - A large number of syntheses methods and tables excist + electrical circuit simulators
    - Butterworth, Chebyshev -filters
- Possible procedure: Full synthesis in the electrical domain and **conversion** to mechanical domain as the last step
  - LC-elements are mapped to lumped mechanical elements
- **Possible, but generally not recommended**
  - → knowledge from both electrical and mechanical domains should be used for **optimal filter design**

2-resonator HF-VHF micromechanical filter



2-resonator HF-VHF micromechanical filter

- The coupled resonator filter may be classified as a 2-port:
  - Two c-c beams
  - 0.1 µm over substrate
    - Determined by thickness of ”sacrificial oxide”
  - Soft coupling spring
  - polySi stripes under each resonator → electrodes
  - Vibrations normal to substrate
  - DC voltage applied
  - polySi at the edges function as tuning electrodes
    - (”beam-softening”)

Resistors

- AC-signal on input electrode through R_{Q1}
  - R_{Q1} reduces Q and makes the pass band more flat
- Matched impedance at output, R_{Q2}
  - R' s may be tailored to specific applications
  - e.g. may be adjusted for interfacing to a following LNA

”Mechanical signal processing”

- Input signal is converted to force
  - By capacitive input transducer

- Mechanical vibrations are induced in x-direction

- The resulting **mechanical signal** is processed in the mechanical domain
  - ”Reject” if outside pass band
  - ”Passed” if inside pass band

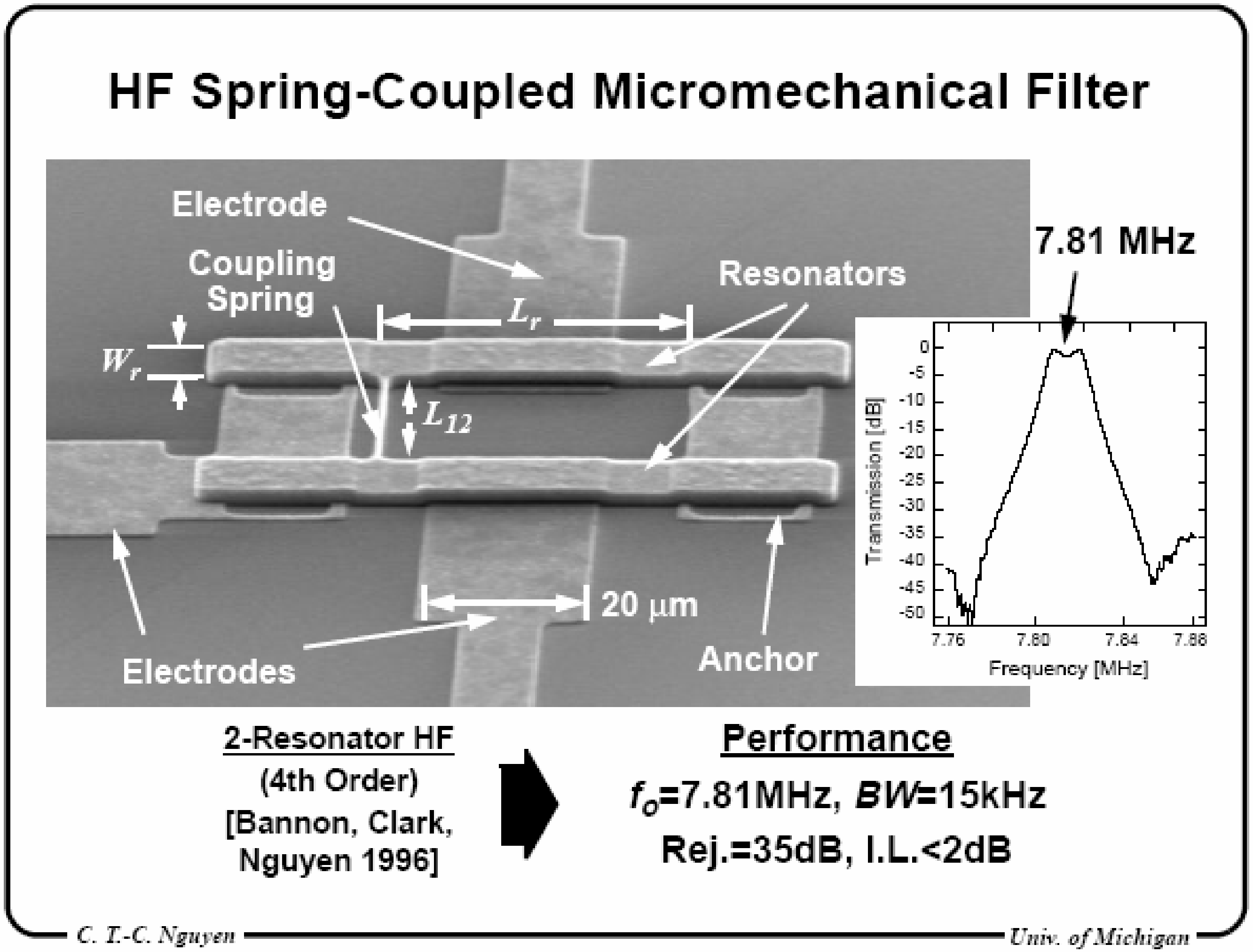
”Mechanical signal processing”, contd.

- The mechanically processed signal manifests itself as movement of the <u>output transducer</u>
- The movement is converted to electrical energy
  - Output current $i_0 = Vd * dC/dt$

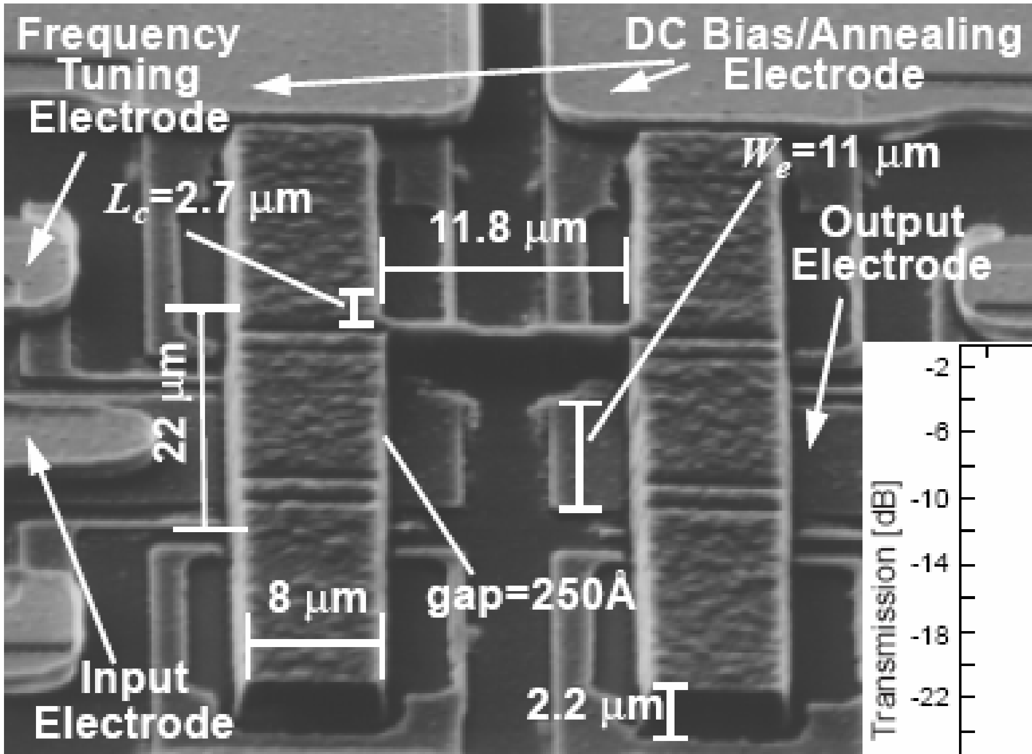
- ➔ **”micromechanical signal processor”**

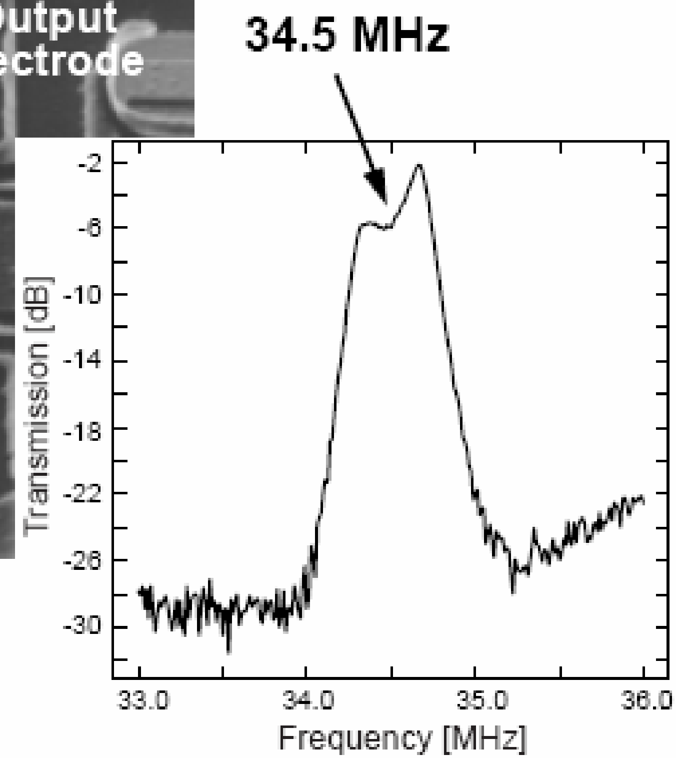
- The electrical signal can be further processed by succeeding transceiver stages

BP-filter using 2 c-c beam resonators



VHF Spring-Coupled Micromechanical Filter





Performance:

V_P~15V, R_Q~2kΩ

f_o~34.5MHz, BW~1.3%

Rej.=25dB, I.L.<6dB

[Wong, Ding, Nguyen 1998]

Comb structure

- Both series and parallel configurations can be used
- In figure 5.11.b the output currents are added

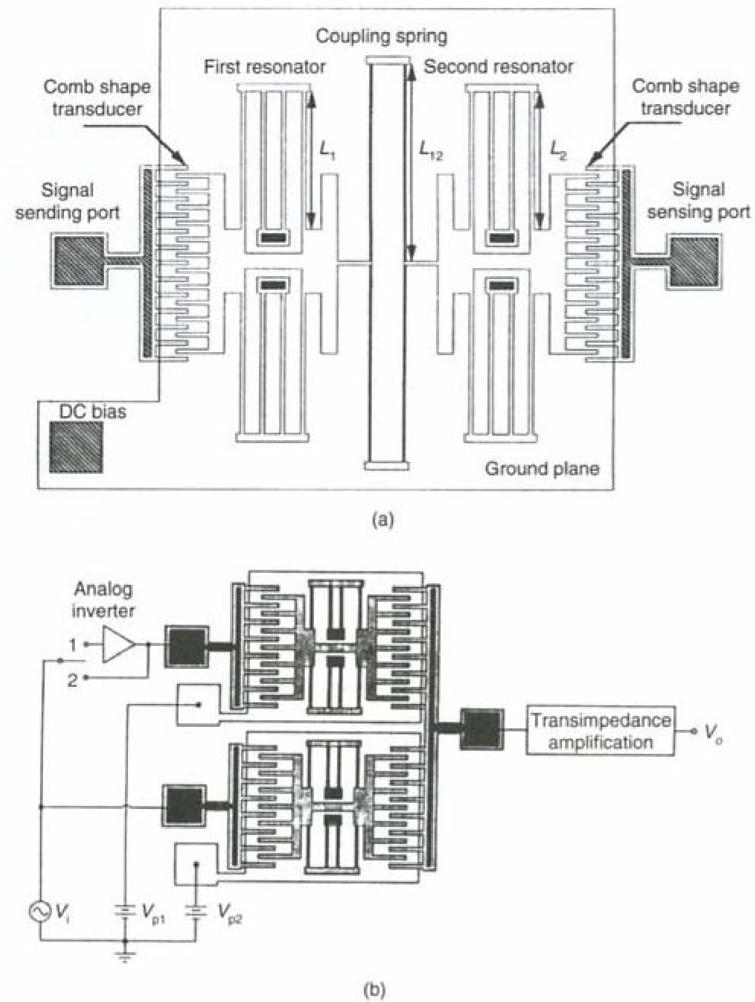


Figure 5.11 (a) Series and (b) parallel combination of resonators. Reproduced from L. Lin, C.T.-C. Nguyen, R.T. Howe, and A.P. Pisano, 1992, 'Micro electromechanical filters for signal processing', in *IEEE Conference on Micro Electro Mechanical Systems '92, February 4–7 1992*, IEEE, Washington, DC, by permission of IEEE, © 1992 IEEE

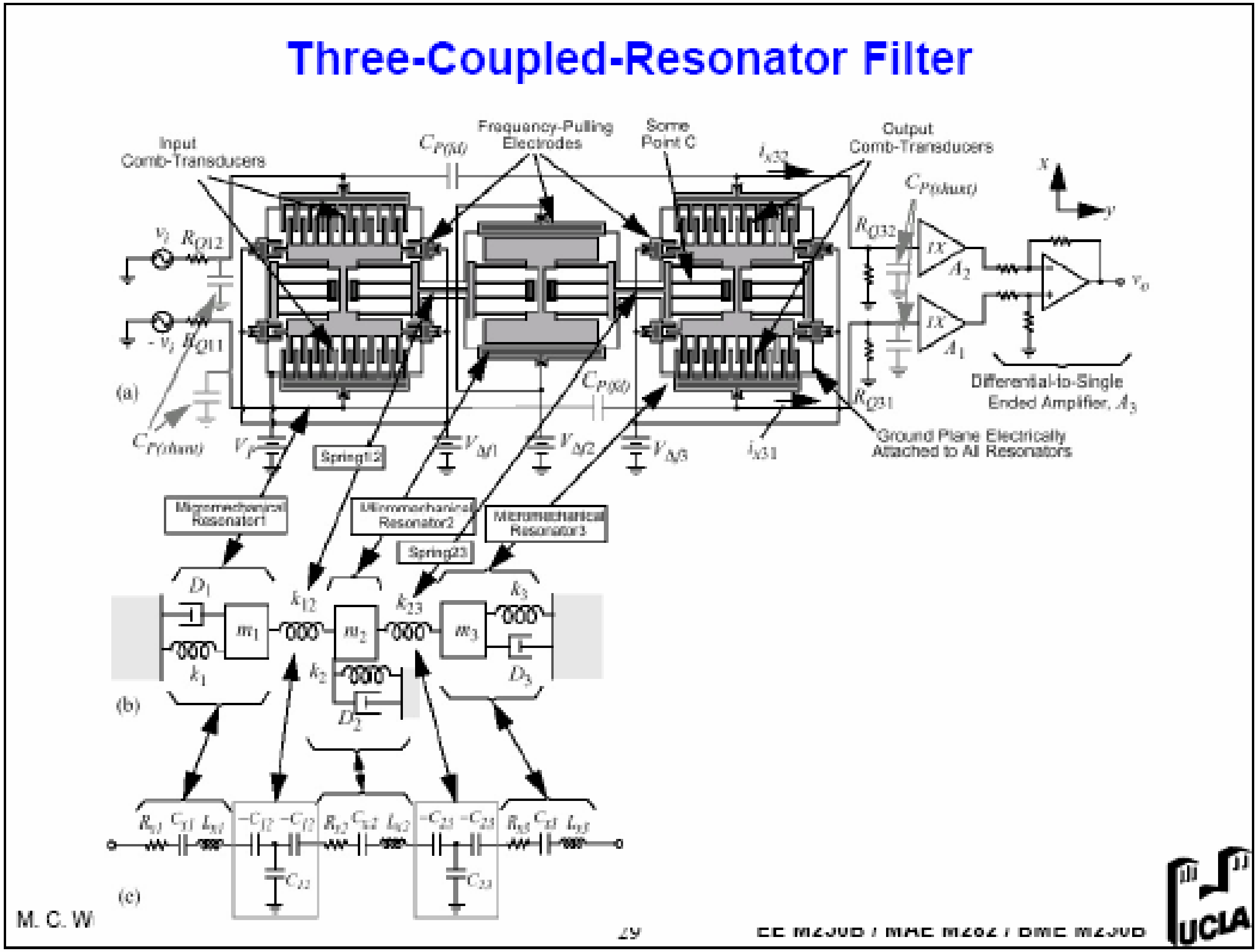
Comb-structure, contd.

- Resonators designed for different resonance frequencies

$$f_2 - f_1 = \frac{f_1}{Q_1}$$

  - Model taken from Varadan p. 262-263:
    - Model assumes a massless coupling beam. Possible to ignore the influence of the mass on the filter performance if the coupling beam length is a **quarter wavelength** of the centre frequency
  - Formulas inaccurate for high frequencies and small dimensions
    - → Better method: Use advanced simulation tools

Filter implemented using comb structure



Three-Resonator Spring-Coupled Filter

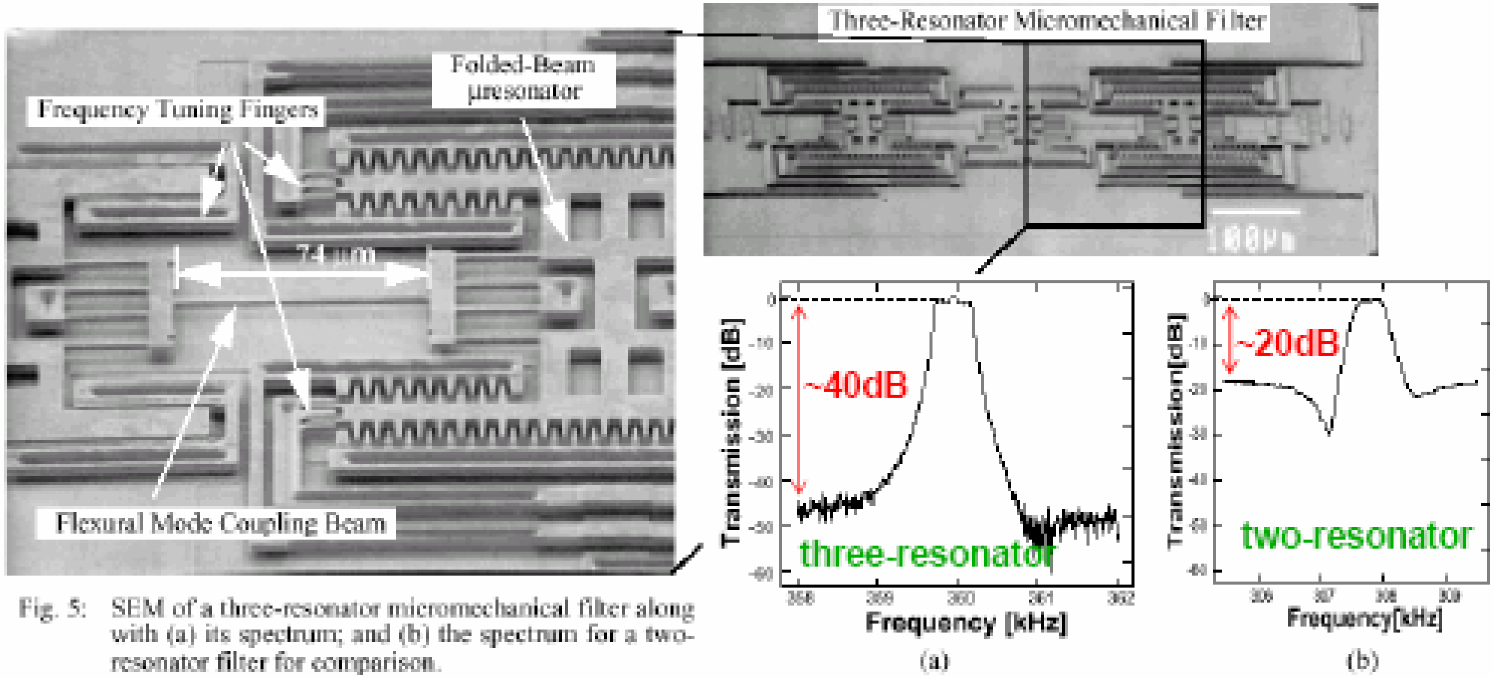
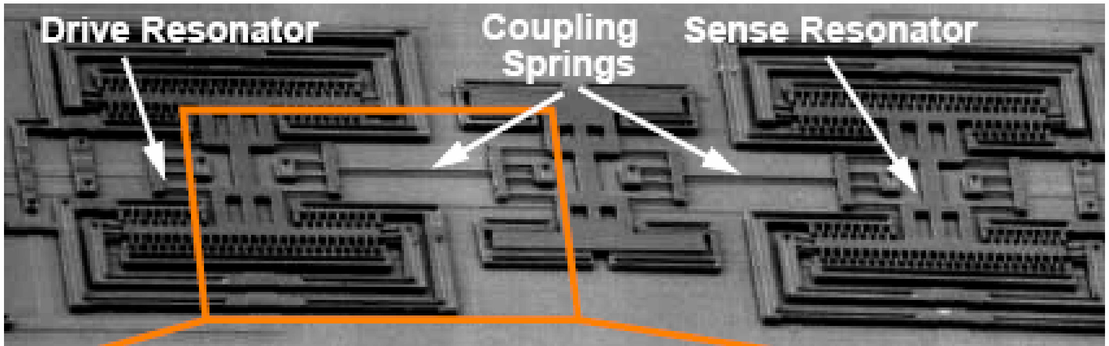


Fig. 5: SEM of a three-resonator micromechanical filter along with (a) its spectrum; and (b) the spectrum for a two-resonator filter for comparison.

High-Order μMechanical Filter



3-Resonator MF

(6th Order, 1/5-Velocity Coupled)

f_0=340kHz

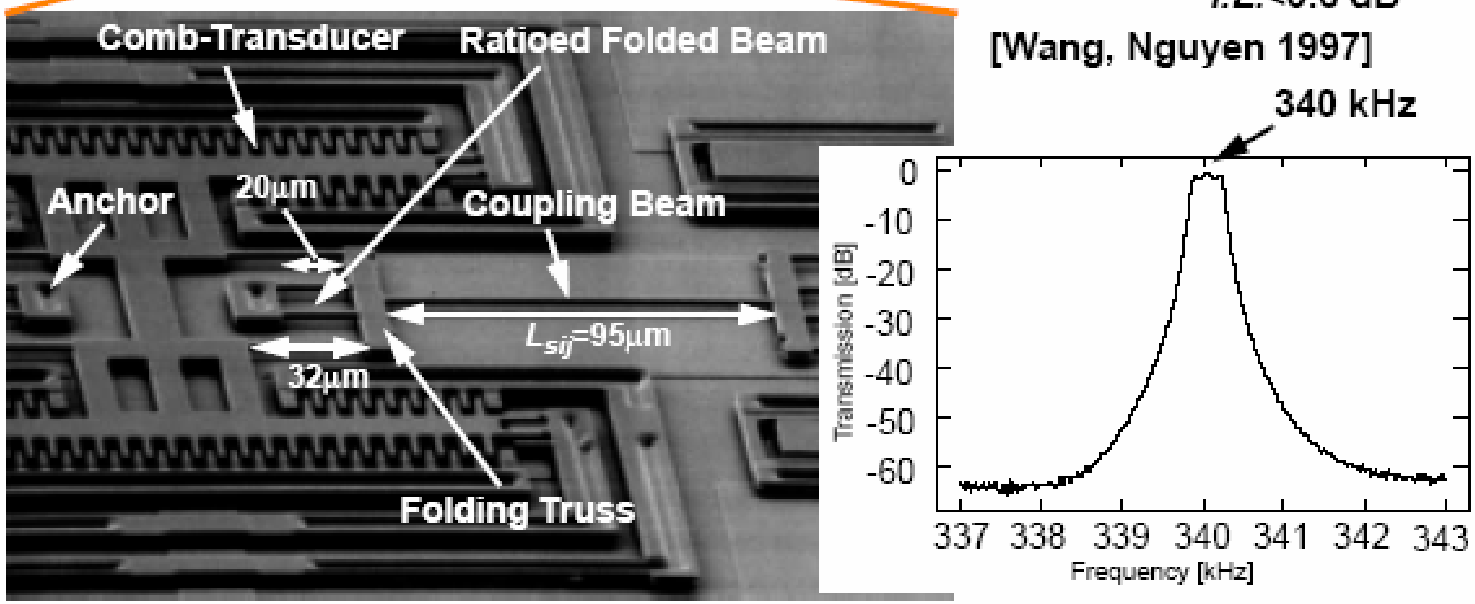
BW=403Hz

%BW=0.09%

Stop.R.=64 dB

I.L.<0.6 dB

[Wang, Nguyen 1997]



Design procedures c-c beam filter

- A. Design resonators first
  - This will give constraints for selecting the stiffness of the coupling beam
  - → bandwidth B can not be chosen freely!

or

- B. Design coupling beam spring constant
  - Determine the spring constant the resonator must have for a given B
  - → this determines the coupling point!

Design procedure A.

- **A1.** Determine resonator geometry for a given frequency and a specific material (ρ)
  - Calculate beam-length (L_r), thickness (h) and gap (d) using equations for f_0 and terminating resistors (R_Q)
    - If filter is symmetric and $Q_{resonator}$ >> Q_{filter}, a simplified model for the resistors may be used →

For a specific resonator frequency, geometry is determined by:

$$f_0 = const \cdot \sqrt{\frac{E}{\rho}} \cdot \frac{h}{L_r^{\,2}} \cdot \left(1 - \left\langle \frac{k_e}{k_m} \right\rangle \right)^{1/2}$$

$h,\ L_r$: determined from f_0 – requirement

$W_r,\ W_e$: chosen as practical as possible

Added requirement : R_Q

$$R_Q = \frac{k_{re}}{\omega_0 \cdot q_1 \cdot Q_{filter} \cdot \eta_e^{\,2}}, \quad Q_{res} \rangle\rangle Q_{filter}$$

k_{re} : given by resonator dimensions

ω_0 : is given

q_1 : from filter cook book

Q_{filter} : is given

$\eta_e = V_P \cdot \frac{\partial C}{\partial x} \approx \frac{V_P}{d^2}$: only possible variation

V_P : has limitations

d : can be changed! (e, is centre position of beam)

Design-procedure A, contd.

- **A2.** Choose a **realistic width** of the coupling beam W_{s12}
- Length of coupling beam should be a quarter wavelength of the filter centre frequency
  - → Coupling springs are in general transmission lines
  - The filter will not be very sensitive to dimensional variations of the coupling beam
  - Quarter wavelength requirement determines the **length of the coupling beam** L_{s12}

Design procedure A, contd.

- Constraints on width, thickness and length determines the **coupling spring constant**

$$k_{s12}$$

  - This limits the possibility to set the bandwidth independently (B depends on the coupling spring constant)

$$B = \left(\frac{f_0}{k_{12}}\right) \cdot \left(\frac{k_{s12}}{k_{rc}}\right)$$

  - An **alternative method for determining the filter-bandwidth** is needed→ see design procedure B.

Design procedure B

- **B1.** Use **coupling points** on the resonator to determine filter bandwidth
  - B determined by the ratio $$\frac{k_{s12}}{k_{rc}}$$
    - k_{rc} is the value of k at the **coupling point!**
    - k_{rc} position dependent, especially of the **speed** at the position
    - k_{rc} **can be selected by choosing a proper coupling point of resonator beam!**
- The dynamic spring constant k_{rc} for a c-c beam is largest nearby the anchors
  - k_{rc} **is larger for smaller speed of coupling point at resonance**

Positioning of coupling beam

- So: filter bandwidth can be found by choosing a value of k_r fulfilling the equation

$$B = \left(\frac{f_0}{k_{ij}}\right) \cdot \left(\frac{k_{sij}}{k_r}\right)$$

  – where k_{sij} is **given** by the quarter wavelength requirement

- Choice of **coupling point of resonator beam** influences on the bandwidth of the mechanical filter →

Position of coupling beam

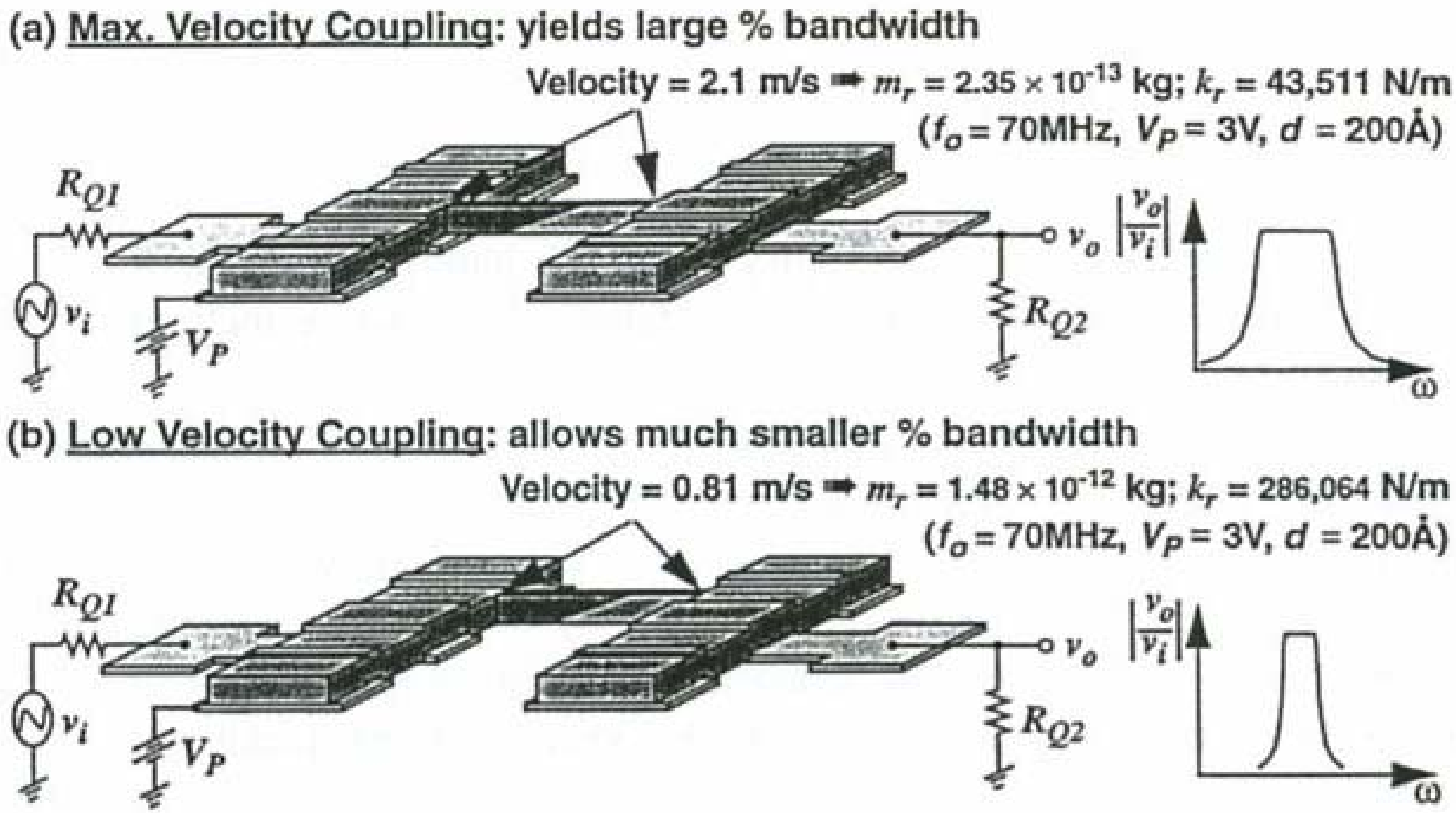
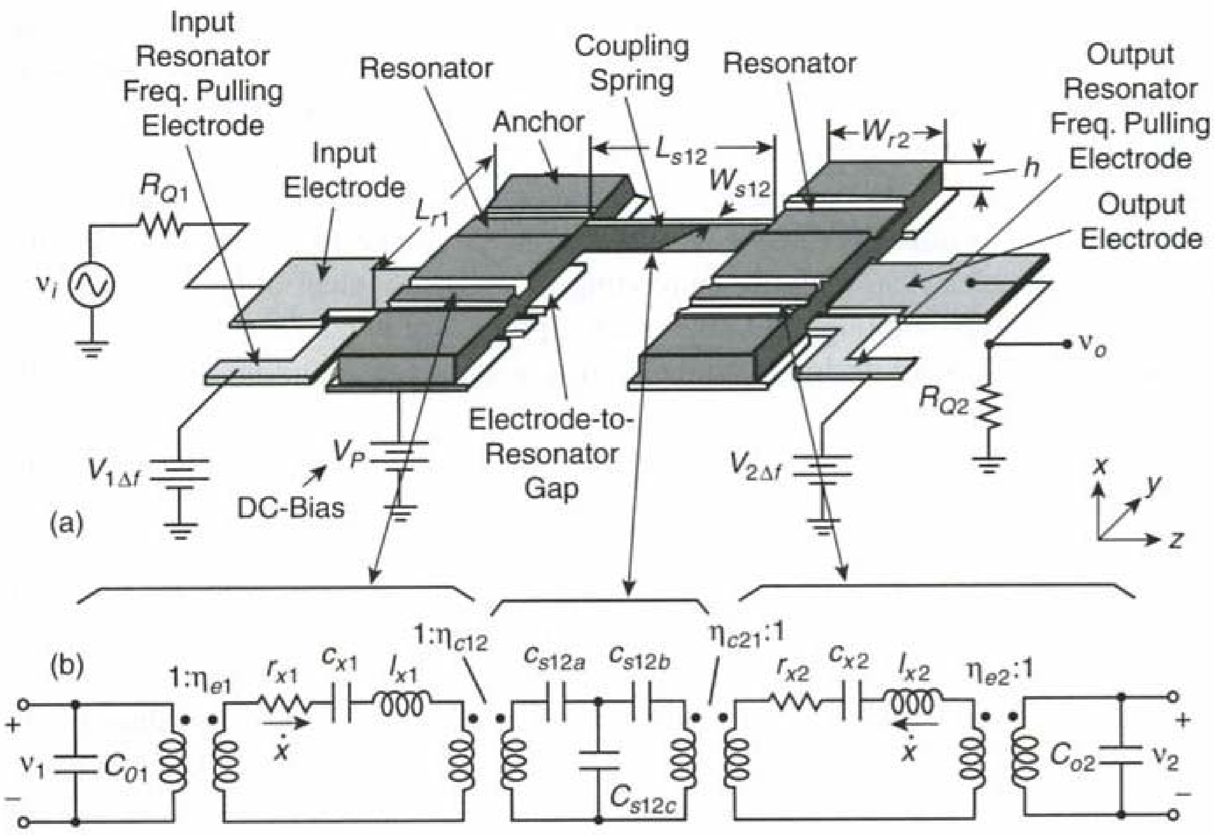


Figure 12.15. Filter schematics showing (a) maximum velocity coupling to yield a large percent bandwidth and (b) low-velocity coupling to yield a smaller percent bandwidth.

Design-procedure, contd.

- **B2.** Generate a complete equivalent circuit for the whole filter structure and verify using a circuit simulator
  - Equivalent circuit for 2-resonator filter
  - Each resonator is modeled as shown before
  - Coupling beam operates as an acoustic transmission line and is modeled as a T-network of energy storing elements
    - Transformers are placed in-between resonator and coupling beam circuit to model velocity transformations that take place when coupling beam is connected at positions outside the resonator beam centre



η_{ei} = Eq. (20) | $\eta_{cij} = \sqrt{\frac{k_{ric}}{k_{rie}}}$ | $r_{xi} = c_{rie}$, $l_{xi} = m_{rie}$ | $c_{xi} = \frac{1}{k_{rie}}$ | $c_{sija} = c_{sijb} = \frac{1}{k_{sija}}$ | $c_{sijc} = \frac{1}{k_{sijc}}$ | $c_{oi} = \frac{\varepsilon_o W_r W_e}{d}$

Figure 12.14. (a) Perspective-view schematic of a symmetrical two-resonator VHF μmechanical filter with typical bias, excitation, and signal conditioning electronics. (b) Electrical equivalent circuit for the filter in (a) along with equations for the elements [18]. Here, m_{rie}, k_{rie}, and c_{rie} denote the mass, stiffness, and damping of resonator i at the beam center location, and η_e and η_c are turns ratios modeling electromechanical coupling at the inputs and mechanical impedance transformations at low-velocity coupling locations. (From reference [18])

SEM of symmetric filter: 7.81 MHz

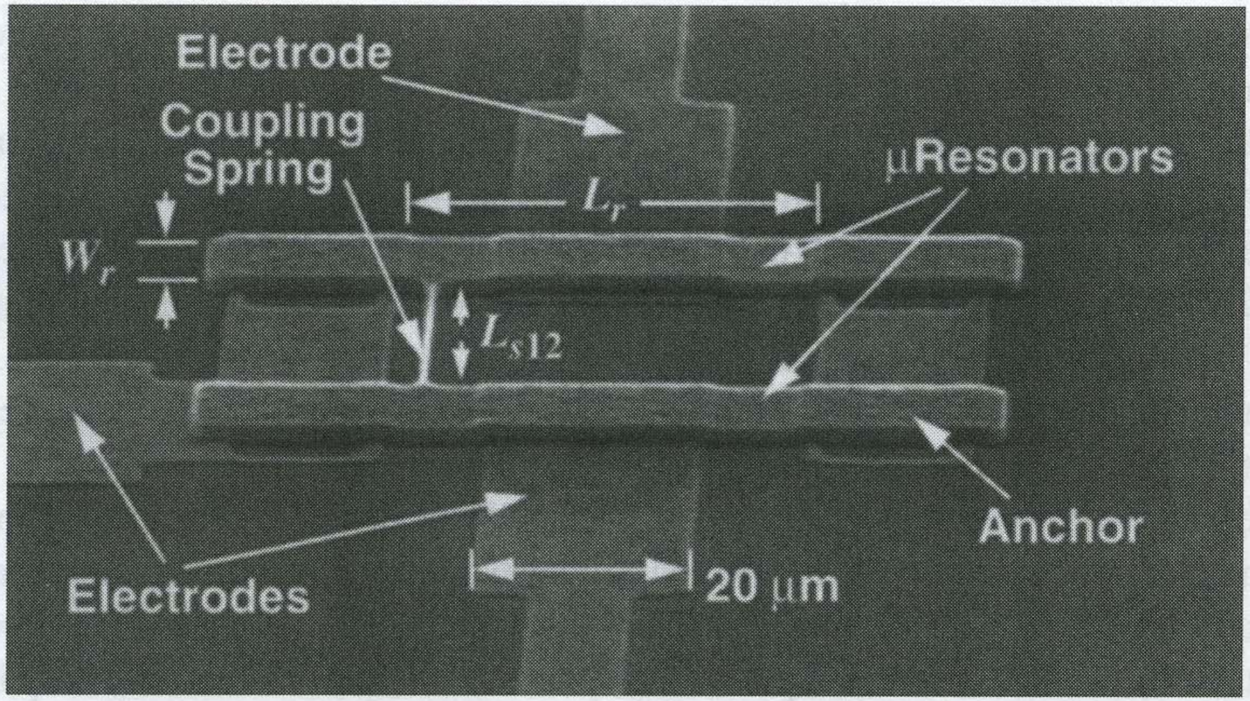


Figure 12.16. SEM of a fabricated 7.81 MHz two-resonator micromechanical filter. (From reference [18])

- Resonators consist of phosphor doped poly

Measured and simulated frequency response

- BW = 18 kHz, Insertion loss = 1.8 dB, Q_filter = 435

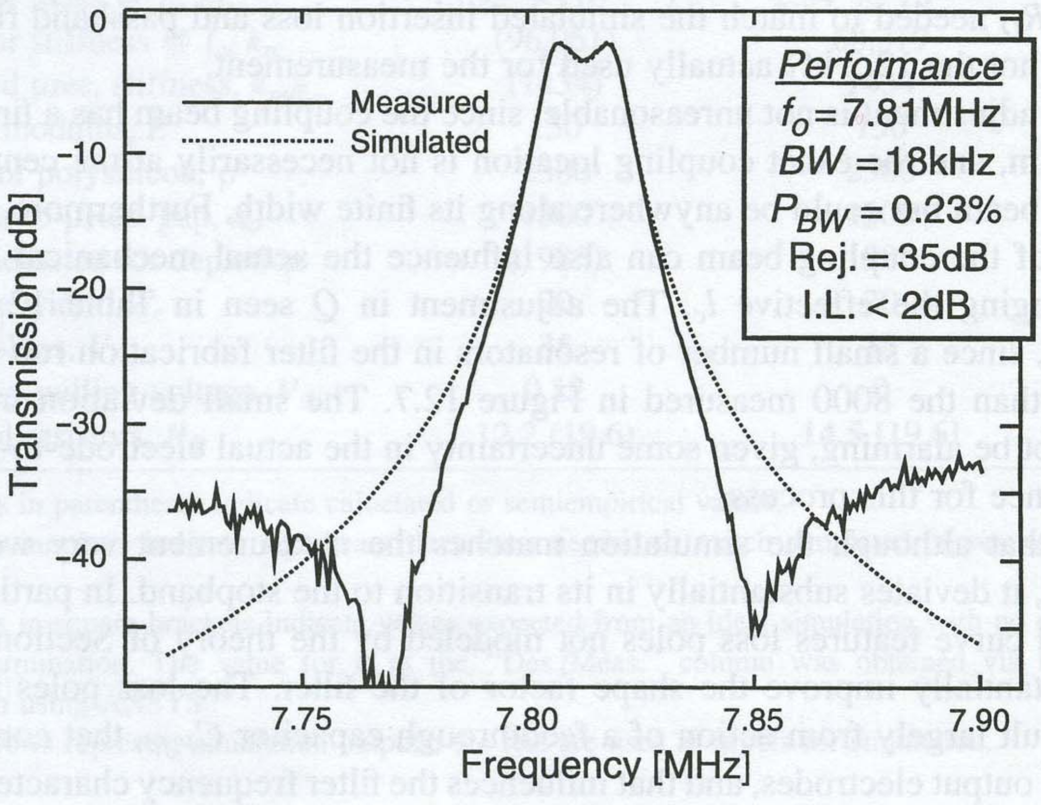


Figure 12.17. Measured spectrum for a terminated 7.81 MHz μmechanical filter with excessive input/output shunt capacitance. Here, $Q_{fltr} = 435$. (From reference [18])

HF micromechanical filter

- Comments to fig. 12.16 and 12.17:
- Coupling position l_c was adjusted to obtain the required bandwidth
  - Torsion rotation of coupling beam may also influence the mechanical coupling
    - Effective value of l_c changes
- Simulation and experimental results match well in pass band
  - Large difference in the transition region to the stop band
    - In a real filter **poles** that are not modeled, are introduced. They improve the filter shape factor. Due to the feed-through capacitance C_p between input and output electrodes (parasitic element). For fully integrated filters this capacitance can be controlled and the position of the poles can be chosen such that they contribute to a optimized filter performance

Micromechanical mixer filters

- A 2 c-c beam structure can be modified to be a **mixer**
  - Suppose input signals on both on v_e (electrode) and v_b (beam)

- Fig 12.18 Itoh, shows schematic for a symmetric micromechanical mixer-filter-structure →

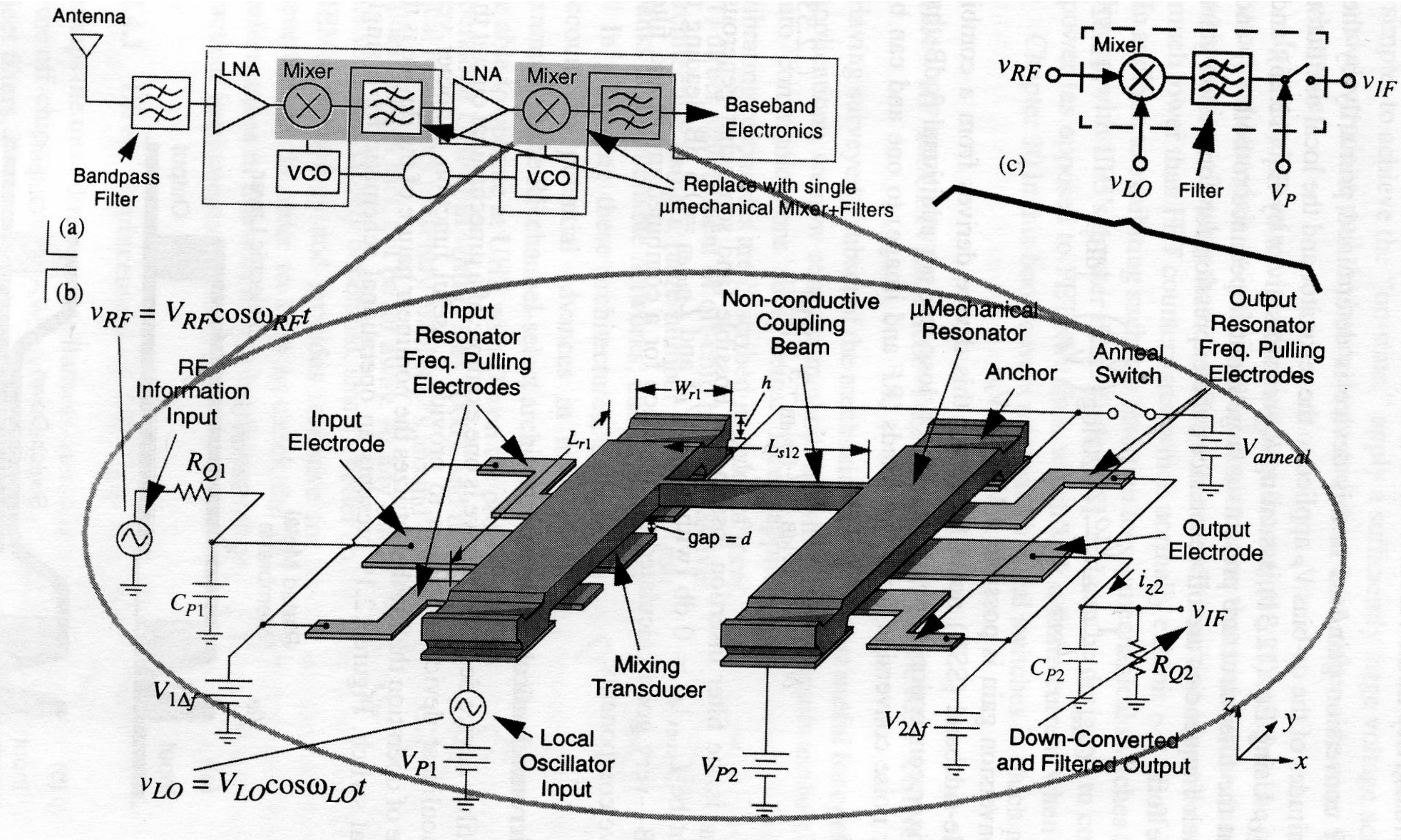


Figure 12.18. (a) Simplified block diagram of a wireless receiver, indicating (with shading) the components replaceable by mixer-filter devices. (b) Schematic diagram of the described μmechanical mixer–filter, depicting the bias and excitation scheme needed for downconversion. (c) Equivalent block diagram of the mixer–filter scheme.

Mixer

Suppose v_{RF} on electrode

Suppose local oscillator on beam, $v_b = v_{LO}$

Force calculated :

$$F_d = \frac{1}{2}(v_e - v_b)^2 \frac{\partial C}{\partial x} = \frac{1}{2}(v_b{}^2 - 2v_b v_e + v_e{}^2)\frac{\partial C}{\partial x}$$

Suppose : $v_e = v_{RF} = V_{RF} \cos \omega_{RF} t$

$$v_b = v_{LO} = V_{LO} \cos \omega_{LO} t$$

$$F_d = \ldots - \frac{1}{2} \cdot 2V_{LO}V_{RF} \frac{\partial C}{\partial x} \cdot \cos \omega_{LO} t \cdot \cos \omega_{RF} t$$

[where $2\cos \omega_1 t \cdot \cos \omega_2 t = \cos(\omega_1 - \omega_2)t + \cos(\omega_1 + \omega_2)t$]

$$F_d = \ldots - \frac{1}{2} V_{RF} V_{LO} \frac{\partial C}{\partial x} \cdot \cos(\omega_{RF} - \omega_{LO})t$$

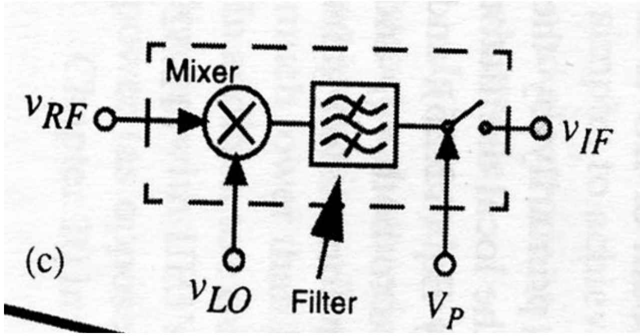
$$F_d = \ldots \;\; \ldots\ldots\ldots\ldots\ldots\ldots \cdot \cos \omega_{IF} t$$

Micromechanical mixer filters, contd.

- Summary of calculations
  - Start with a non-linear relationship between voltage and force: voltage/force characteristic (square)
  - Linearization: Vp suppresses non-linearity
  - Voltage signals v_{RF} and v_{LO} are mixed down to intermediate frequency (force), ω_{IF} = difference between frequencies!

- Transducer no. 1 can couple the signal into the following resonator
  - If transducer no. 2 is designed as a micromechanical BP filter with centre frequency ω_{IF}, we will get an effective **mixer-filter structure**

Micromechanical mixer-filter, contd.



- → Mixer structure is a **functional-block in a RF-system** (future lecture)
  - This is a component that may replace present mixer + IF-filter (intermediate-filter)
  - Lower contact-loss between parts and ideally zero DC power consumption
    - A non-conducting coupling beam is used for isolating the IF-port from LO (local oscillator)