

## TWO-DIMENSIONAL METAMATERIAL

We have already seen how the concept of a metamaterial yields an analytic description of a planar periodic layer structure. Now let us apply the metamaterial concept to a doubly periodic array of cylinders. Let the relative permittivity be  $\varepsilon_1$  inside the cylinders and  $\varepsilon_2$  between the cylinders, and let the cylinder radius be  $a$ .

### Problem 1

Let us first consider the case with the E field pointing in the z direction along the cylinders, *i.e.*, transverse magnetic (TM) polarization. In the metamaterial (low-frequency) limit, the E field is then approximately constant inside a unit cell of the photonic crystal. The **effective relative permittivity**  $\varepsilon_{zz}$  of the metamaterial is defined as the mean of the D field over the unit cell divided by the mean of the E field times  $\varepsilon_0$  over the unit cell. Show that for a z-polarized field,

$$\varepsilon_{zz} = \varepsilon_2 + (\varepsilon_1 - \varepsilon_2) f, \quad (1)$$

where the fill factor  $f$  is the area of the cylinder relative to the area of the unit cell,

$$f = \pi a^2 / A_u = \pi a^2 / (bh). \quad (2)$$

The area  $A_u$  of the unit cell is the base line  $b$  times the height  $h$ .

### Problem 2

Let us then consider a TE-polarized field, with the E field lying in the x-y plane, perpendicular to the cylinders, again in the metamaterial limit. Limiting our analysis to a small fill factor, we may consider the E field to be approximately constant inside and between the cylinders. There is then a region near the outside of each cylinder where the field is not constant, and where we may use the low-frequency approximation that the E field is the gradient of a potential  $V(r, \varphi)$  that is continuous everywhere, and has the form

$$V_1(r, \varphi) = -E_0 \frac{2\varepsilon_2}{\varepsilon_2 + \varepsilon_1} r \cos \varphi = -E_0 \frac{2\varepsilon_2}{\varepsilon_2 + \varepsilon_1} x \quad \text{for } r < a \quad (\text{inside the cylinder}) \quad (3)$$

$$V_2(r, \varphi) = -E_0 \left( r + \frac{\varepsilon_2 - \varepsilon_1}{\varepsilon_2 + \varepsilon_1} \frac{a^2}{r} \right) \cos \varphi = \quad (4)$$

$$= -E_0 \left( x + \frac{\varepsilon_2 - \varepsilon_1}{\varepsilon_2 + \varepsilon_1} \frac{a^2 x}{x^2 + y^2} \right) \quad \text{for } r > a \quad (\text{outside the cylinder}) \quad (5)$$

Show that the potential (3) inside the cylinder yields a constant E field that points in the x direction and is equal to

$$E_{x,1} = \frac{2\varepsilon_2}{\varepsilon_2 + \varepsilon_1} E_0. \quad (6)$$

### Problem 3

From (5), derive expressions for the x and y components of the E field outside the cylinder with radius  $a$ . Show that the mean of the E field points in the x direction, when the mean is taken over the cross-sectional area outside the cylinder of radius  $a$  and inside the rectangular unit cell. Show that this mean is equal to  $E_0$ , regardless of the size of the unit cell.

#### Problem 4

Show that when the cylinders are far from each other, we get the following approximations for the means of  $E_x$  and  $D_x$  over the unit cell,

$$\bar{E}_x = \left(1 + \frac{\varepsilon_2 - \varepsilon_1}{\varepsilon_2 + \varepsilon_1} f\right) E_0, \quad (7)$$

$$\bar{D}_x = \varepsilon_2 \varepsilon_0 \left(1 - \frac{\varepsilon_2 - \varepsilon_1}{\varepsilon_2 + \varepsilon_1} f\right) E_0, \quad (8)$$

resulting in the effective relative permittivity

$$\varepsilon_{xx} \approx \varepsilon_2 \left(1 - \frac{2(\varepsilon_2 - \varepsilon_1)}{\varepsilon_2 + \varepsilon_1} f\right). \quad (9)$$

#### Problem 5

Now let us consider the general case with cylinders that are not far from each other, but restrict ourselves to a rectangular unit cell with width  $b$  and height  $h$ . We note that if the E field is x-polarized in the center of the cylinder in a rectangular unit cell, the E field is purely x polarized in all the mirror planes of the structure, x-z planes and y-z planes going through the centers of the cylinders and in the middle between cylinders. We note that everywhere inside the unit cell,

$$r < d = \frac{1}{2}\sqrt{b^2 + h^2}. \quad (10)$$

Instead of a single cosine contribution like in (3), we then need a sum of cosine terms, a so-called multipole expansion, to represent the E field, both inside and outside the cylinder. Inside the cylinder (for  $r < a$ ) we may use the following expressions for the x and y components of the E field

$$E_{x,1}(r, \varphi) = \sum_{m=0}^{M-1} E_m \frac{2\varepsilon_2}{\varepsilon_2 + \varepsilon_1} \frac{r^{2m}}{d^{2m}} \cos(2m\varphi), \quad (11)$$

$$E_{y,1}(r, \varphi) = -\sum_{m=0}^{M-1} E_m \frac{2\varepsilon_2}{\varepsilon_2 + \varepsilon_1} \frac{r^{2m}}{d^{2m}} \sin(2m\varphi). \quad (12)$$

The corresponding expressions for the E field outside of the cylinders (for  $r > a$ ) are

$$E_{x,2}(r, \varphi) = \sum_{m=0}^{M-1} E_m \left( \frac{r^{2m}}{d^{2m}} \cos(2m\varphi) - \frac{\varepsilon_2 - \varepsilon_1}{\varepsilon_2 + \varepsilon_1} \frac{a^{4m+2}}{d^{2m} r^{2m+2}} \cos(2m\varphi + 2\varphi) \right), \quad (13)$$

$$E_{y,2}(r, \varphi) = -\sum_{m=0}^{M-1} E_m \left( \frac{r^{2m}}{d^{2m}} \sin(2m\varphi) - \frac{\varepsilon_2 - \varepsilon_1}{\varepsilon_2 + \varepsilon_1} \frac{a^{4m+2}}{d^{2m} r^{2m+2}} \sin(2m\varphi + 2\varphi) \right). \quad (14)$$

We note that for an x-polarized field in a rectangular unit cell, only terms with even multiples  $2m$  of the angle  $\varphi$  are needed in the multipole expansions (11)-(14).

Show that with  $E_x$  and  $E_y$  given by the multipole expansions (11)-(14), the average of  $E_y$  over a rectangular unit cell is zero.

#### Problem 6 (Matlab)

We can find the expansion coefficients  $E_m$  in the series (11)-(14) via point matching. So let us require  $E_y(r, \varphi)$  in (14) to be minimized in  $2M - 1$  different positions around the unit cell, given by  $2M - 1$  different values for the angle  $\varphi$

$$\varphi_p = \frac{\pi}{4M} p, \quad p = 1, 2, \dots, (2M - 1). \quad (15)$$

The corresponding distances from the origin are

$$r_p = \frac{b}{2 \cos \varphi_p} \quad \text{if } \tan \varphi_p < h/b \quad \text{and} \quad r_p = \frac{h}{2 \sin \varphi_p} \quad \text{if } \tan \varphi_p > h/b. \quad (16)$$

Use the  $2M - 1$  equations obtained by setting  $E_y(r_p, \varphi_p)/E_0 = 0$  in (14) for  $p = 1, 2, \dots, (2M - 1)$  to set up an overdetermined set of linear equations in Matlab and determine  $E_m/E_0$  for  $m = 1, 2, \dots, (M - 1)$ . Then compute the field in the middle between the cylinders,  $E_x(r = b/2, \varphi = 0)/E_0$ . Do the calculation for  $\varepsilon_1 = 2, \varepsilon_2 = 1$ , and  $M = 10$  terms in the series expansion, for two cases of a rectangular unit cell, a tall cell with  $b = 3a$  and  $h = 4a$ , and a wide cell with  $b = 4a$  and  $h = 3a$ .

Hint: An overdetermined system of linear equations can be solved in Matlab with the help of the matrix divide operation.

Finally, do a numerical average over the unit cell to obtain  $\bar{E}_x$  and  $\bar{D}_x$  for both the tall and the wide unit cells, and compare the numerically computed averages with the formulas (7) and (8).

*Updated 29 October, 2014.*